

Simulating the response of planar photonic structures under the strain of surface acoustic waves

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Outline

Motivation

Surface acoustic wave (SAW) model

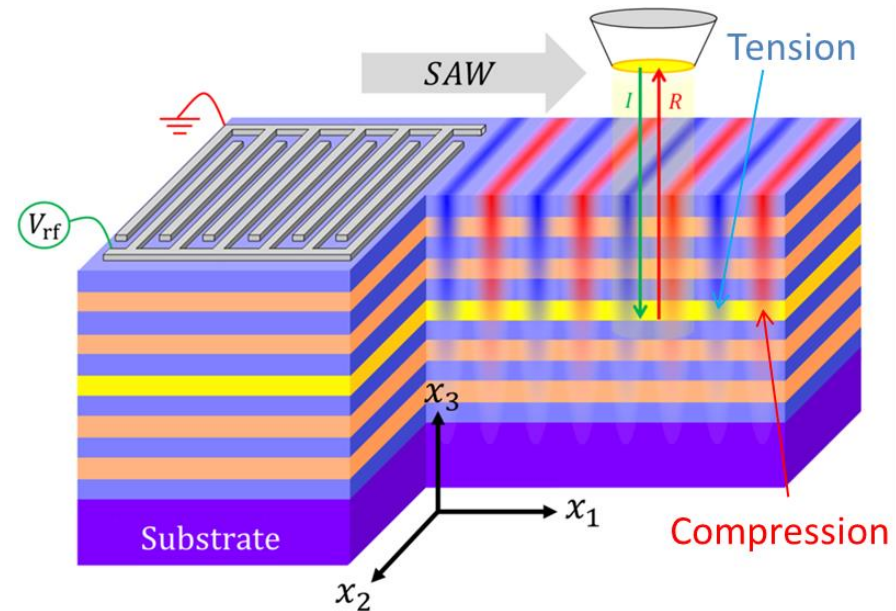
- Calculation of acoustic and piezoelectric properties of solids
 - Bulk, films, layered structures

Planar optical microcavity (POMC) model

- Reflectance spectrum
- Electric field mode confinement
- Quality factor
- Photon dispersion

Acousto-optic modulation model

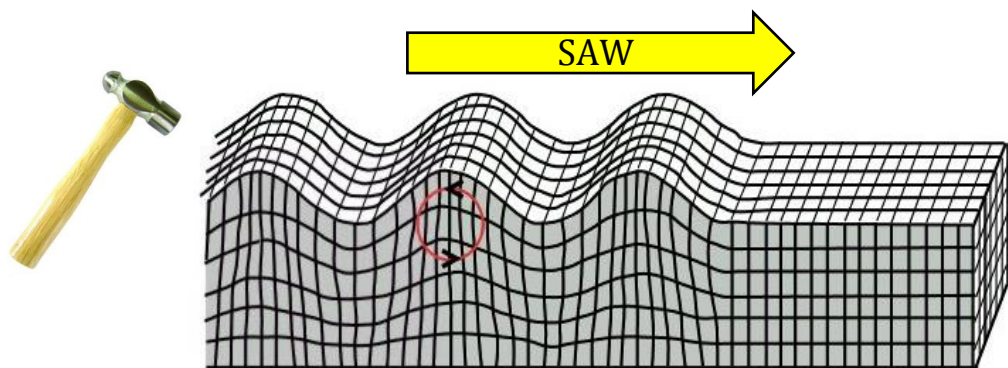
- SAW + POMC
- Strong light-phonon interaction
 - Appearance of new cavity resonances
 - Folding of the photon dispersion
 - Tuning of cavity resonances with SAW strain



Conclusions

Motivation

SAWs: elastic waves propagating on the surface of solids



Modulation of dielectric properties of solids

Applications:

- Mobile, Wireless communication
- Sensors, filters, resonators....

Research

- Long range carrier, spin transport
- Tuning of energy levels in nanostructures

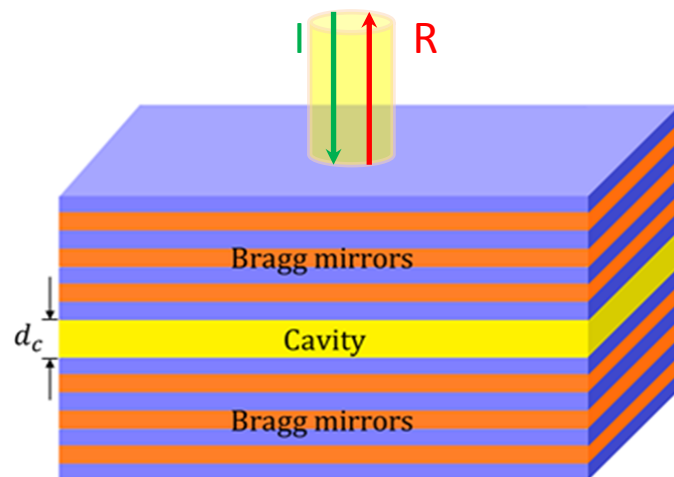
POMC: periodic array of refractive index

- Light confinement in the optical cavity
- Applications in photonics

Enhancement of interaction with light emitters

Light-matter coupling

- Strong coupling
 - Light-matter entangled states
- Weak coupling
 - Emission gain (QDs, nanowires, etc.)



SAWs on piezoelectric crystals

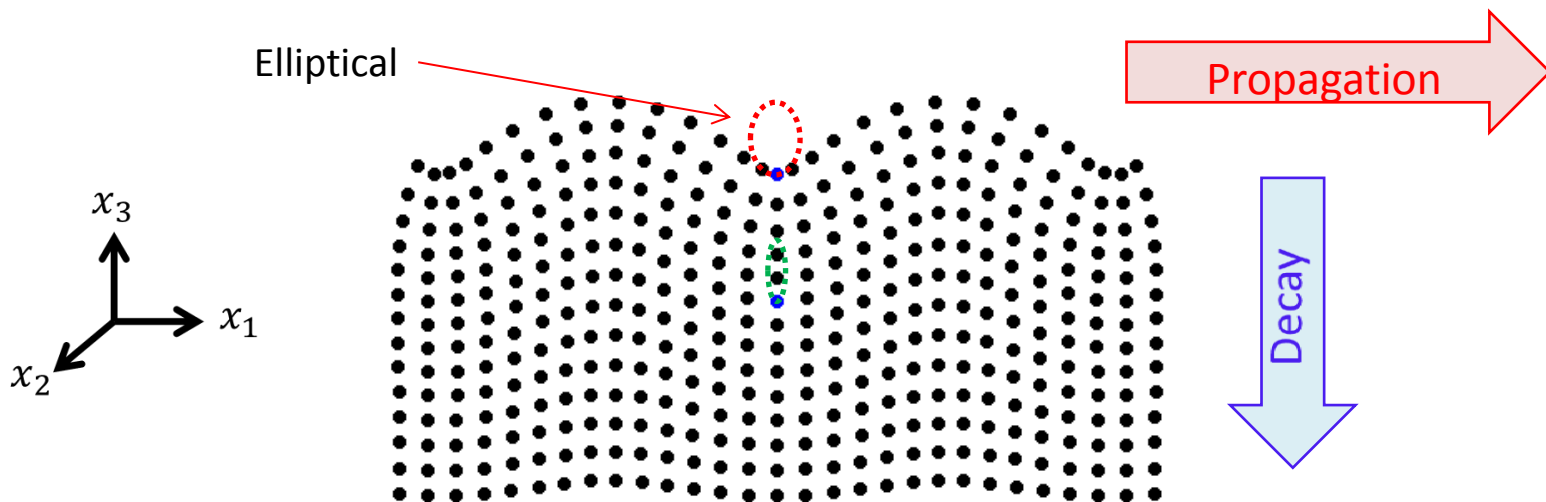
$$T_I = c_{IJ}S_J + d_{kI}E_k \quad (\text{3D Hooke's law} + \text{Converse piezoelectricity})$$

$$D_k = \epsilon_{kl}E_l + d_{kI}S_I \quad (\text{Dielectric field relation} + \text{Direct piezoelectricity})$$

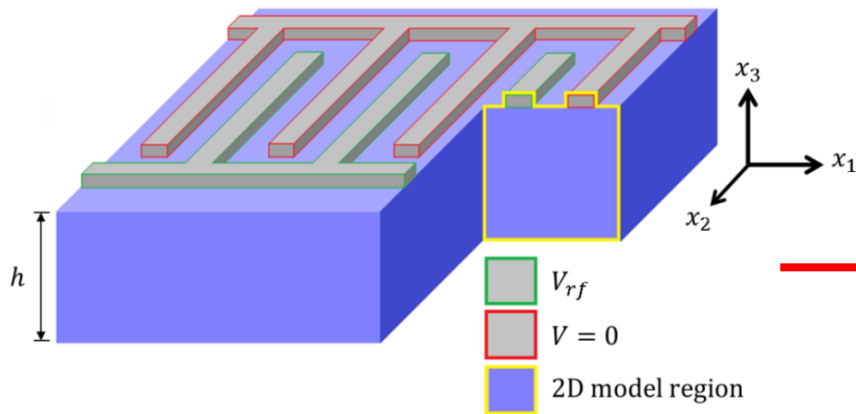
(c_{IJ} , d_{kI} and ϵ_{kl} are tensorial material properties)

SAWs compose a set of solutions to the wave equation

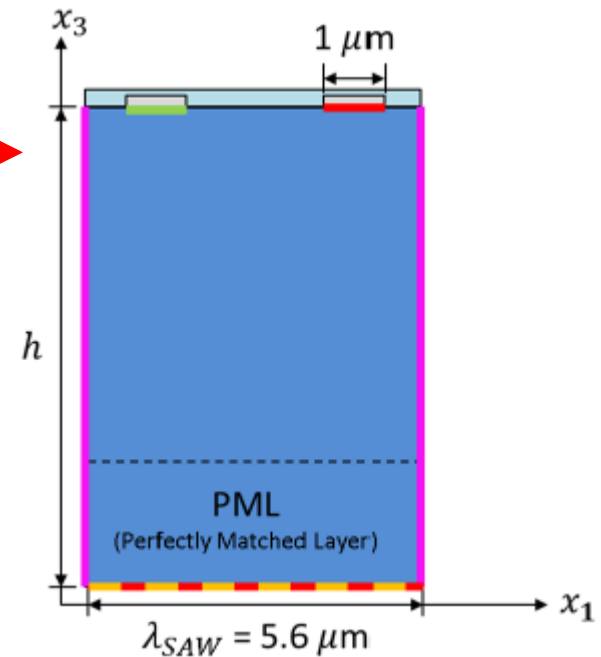
$$\rho \frac{\partial^2 u_i}{\partial t^2} = c_{IJ} \left(\frac{\partial^2 u_l}{\partial x_j \partial x_k} \right) + d_{kI} \left(\frac{\partial^2 \phi}{\partial x_j \partial x_k} \right)$$



2D SAW model



Solid Mechanics module
 Projection into a 2D “unit cell”



Interdigital transducers (IDTs)

- E-shaped aluminium electrodes
- Designed by lithography
- Wavelengths: $\lambda_{SAW} \sim 1 \rightarrow 20 \mu\text{m}$
- Frequencies: $f_{SAW} \sim 0.1 \rightarrow 1 \text{ GHz}$
- $v_{SAW} = \lambda_{SAW} f_{SAW}$

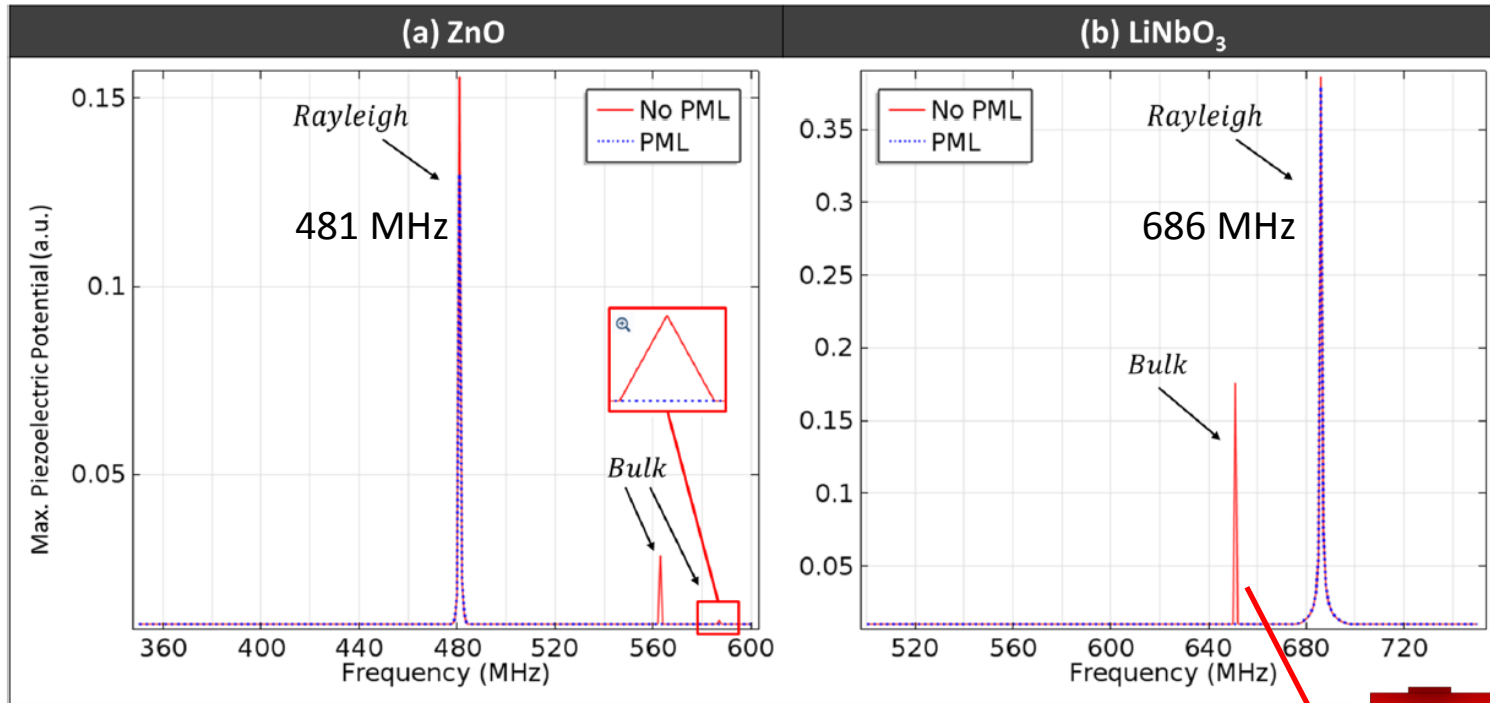
Material	Geometry	Thickness (nm)
Air	Top cover	300
Aluminium	IDTs	200
ZnO/LiNbO ₃	Substrate	14000

Boundary Conditions	
V_{rf}	Applied Electric Potential
$V = 0$	Ground
$ \vec{u} = 0$	Fixed Constraint
Continuity	Periodic Condition

PML: Perfectly Matched Layer → Force solution to decay to the substrate

The SAW model: searching for Rayleigh SAWs

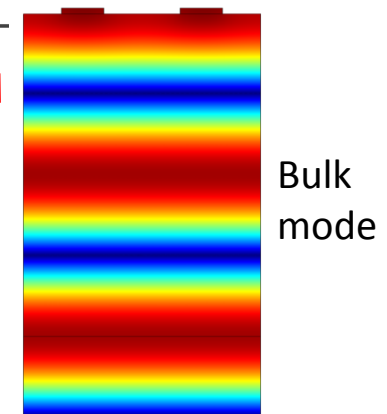
Frequency sweeps seeking for Rayleigh SAWs



Estimated velocities agree well with the literature

$$v^{ZnO} \approx 2694 \text{ m.s}^{-1} \quad v^{LiNbO_3} \approx 3843 \text{ m.s}^{-1}$$

$$* v^{ZnO} \approx 2700 \text{ m.s}^{-1} \quad ** v^{LiNbO_3} \approx 3900 \text{ m.s}^{-1}$$



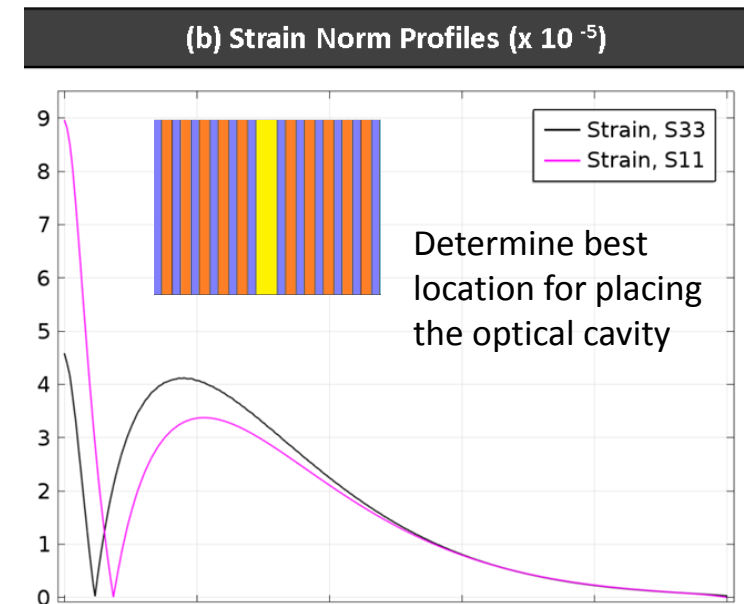
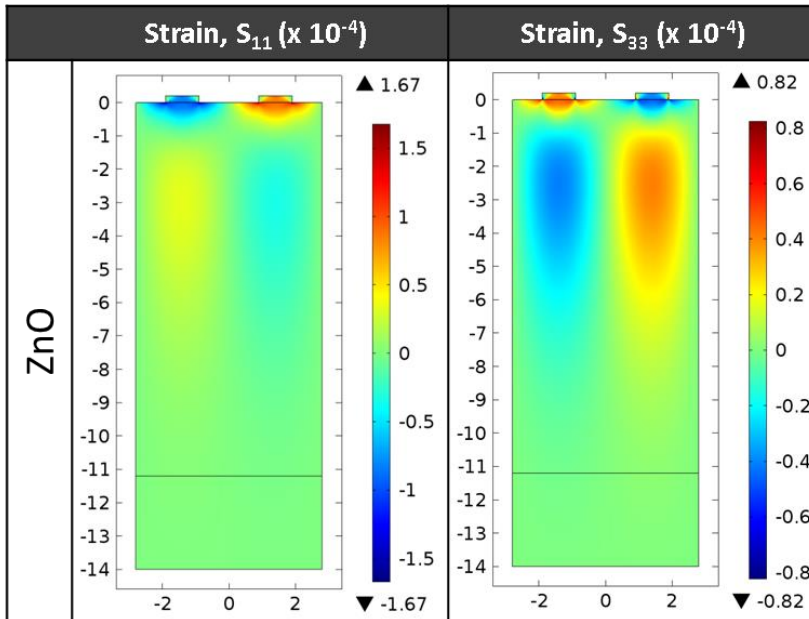
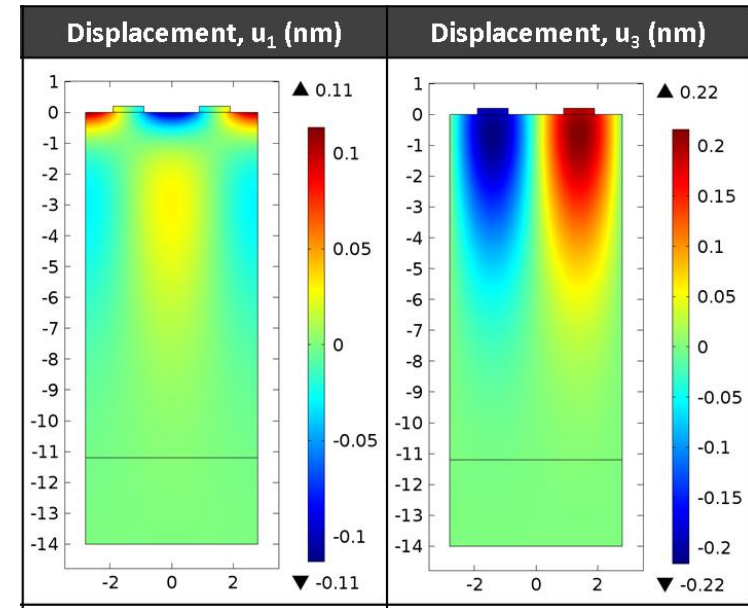
The SAW model eigenmodes: ZnO ($f_{\text{saw}} = 481$ MHz)

Rayleigh SAW modes obtained

- Waves confined at the surface
- Exponential decay to the substrate
- u_1 and u_3
 - Elliptical displacement
 - Phase difference = $\pi/2$

Strain modulation

- Typical values: 10^{-5} to 10^{-3}
- S_{33} : main responsible for the modulation of POMCs

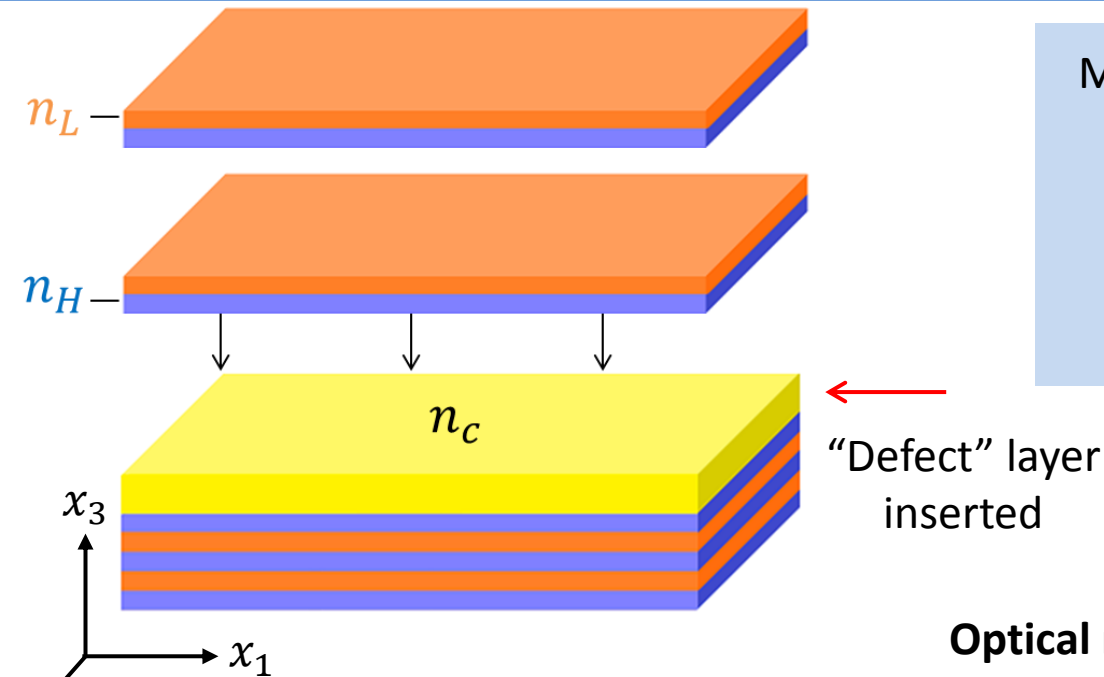


The planar optical microcavity

Maximum reflectance and PBG width:

$$n_c d_c = \frac{\lambda_0}{2}$$

$$n_H d_H = n_L d_L = \frac{\lambda_0}{4}$$

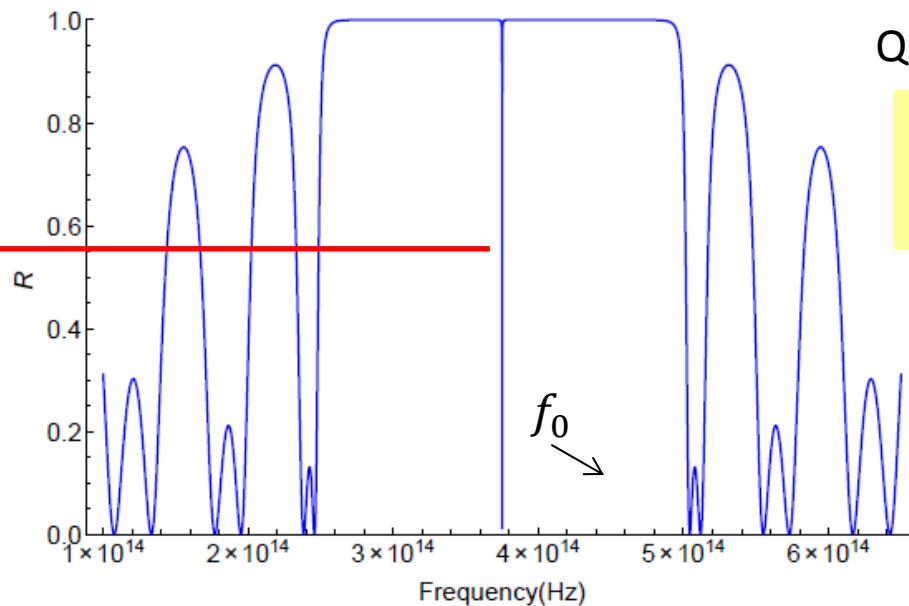
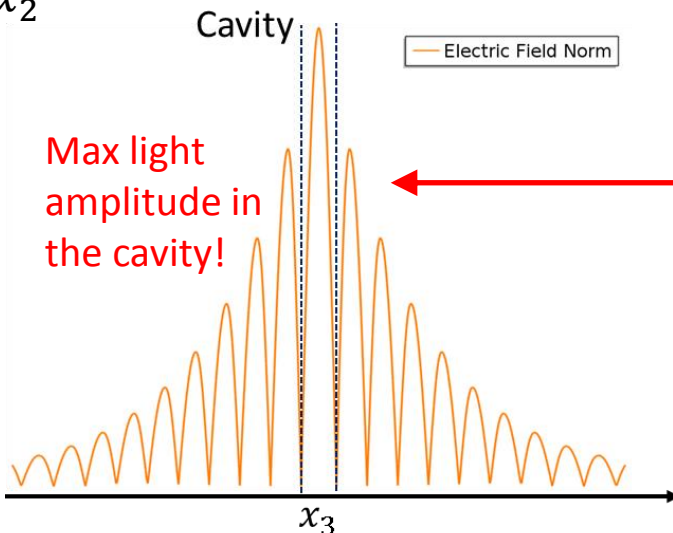


“Defect” layer inserted

Optical resonance appears!

Quality factor

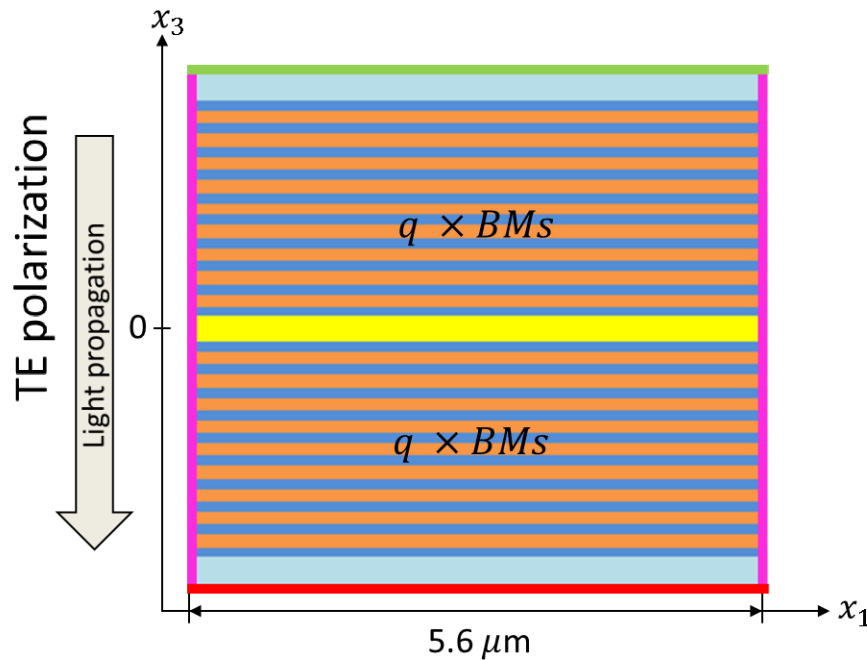
$$Q = \frac{f_0}{\Delta f_0}$$



The POMC model

Electromagnetic waves module

800nm POMC with Bragg mirrors composed of either ZnO/SiO₂



Material	Ref. index	Thickness (nm)
Air	1	300
ZnO	1.974	101.32
LiNbO ₃	2.175	91.95
SiO ₂	1.453	137.65
SiO ₂	1.453	275.29

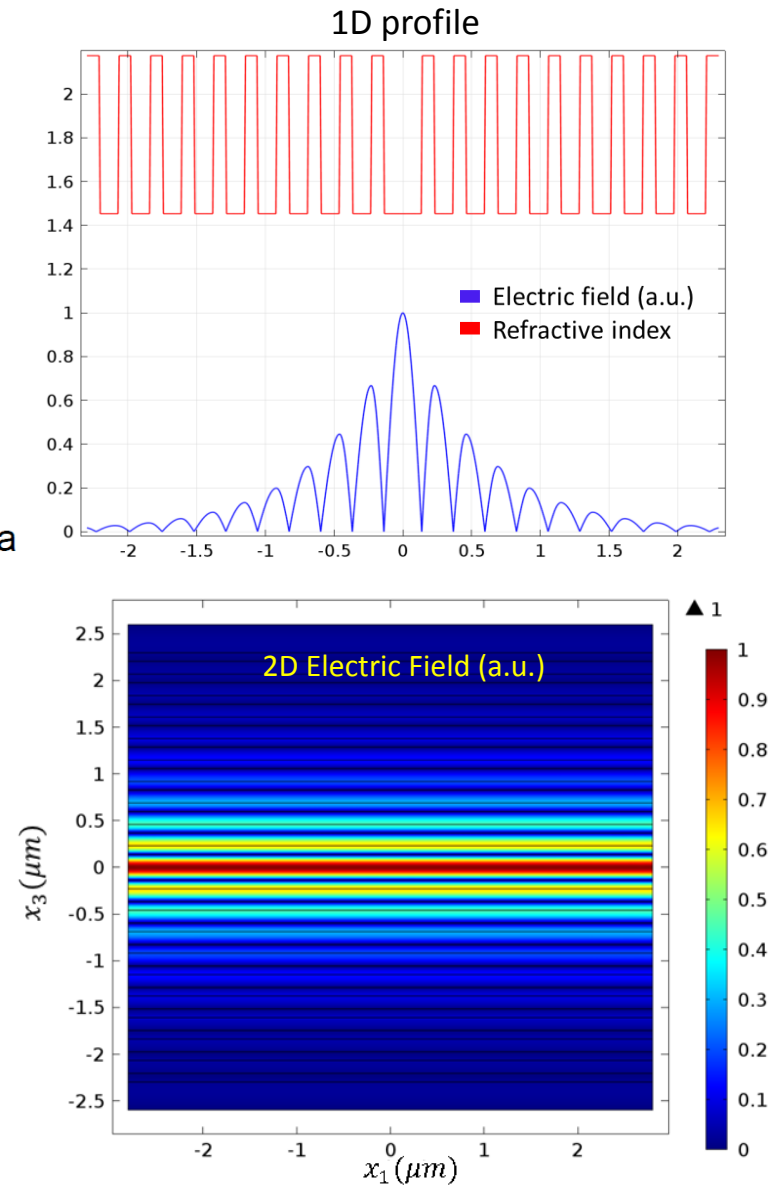
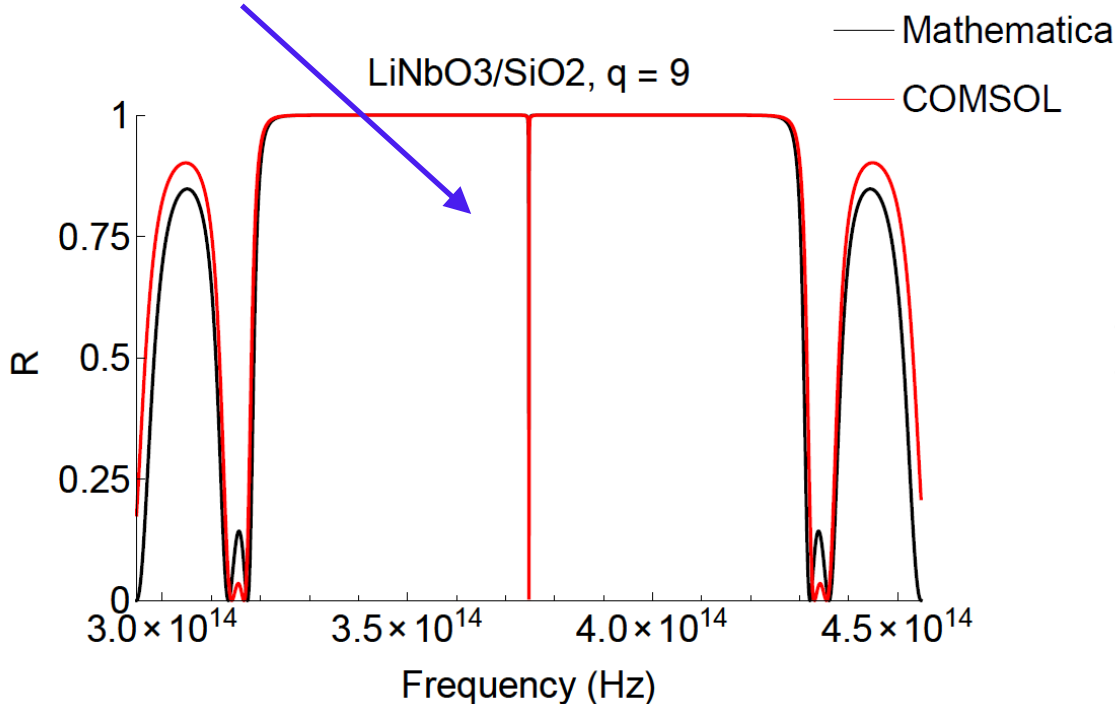
Boundary Conditions	
Port 1	Light excitation, measure of R
Port 2	Light absorption, measure of T
Continuity	Floquet periodicity

- SiO₂: good ref. index contrast with ZnO and LiNbO₃, compatible with CMOS
- Frequency Sweeps: obtain the spectral curves of reflectance
- Angle resolved reflectance: periodic port
- Eigenvalue solver: light electric field components
- Normalization factor: maximum electric field in the cavity

The planar optical microcavity model: results

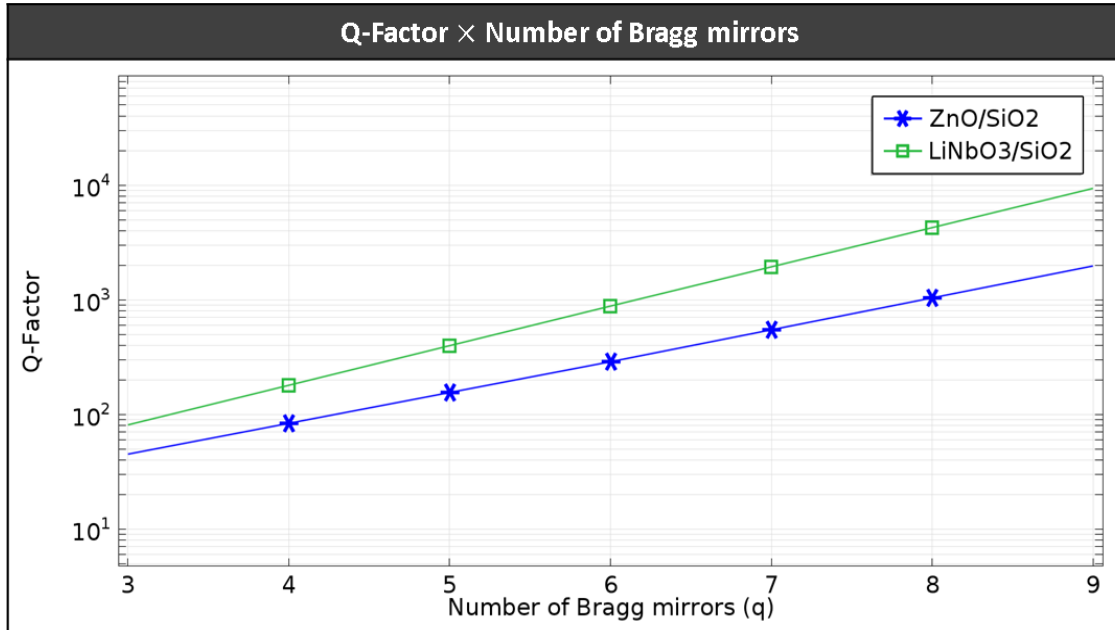
800nm POMC

- Reflectance obtained
- PBG characterized
- Predicted resonance frequency 374.74 THz
- Electric field confinement
 - 1D and 2D plots
- Very good agreement to the TM method

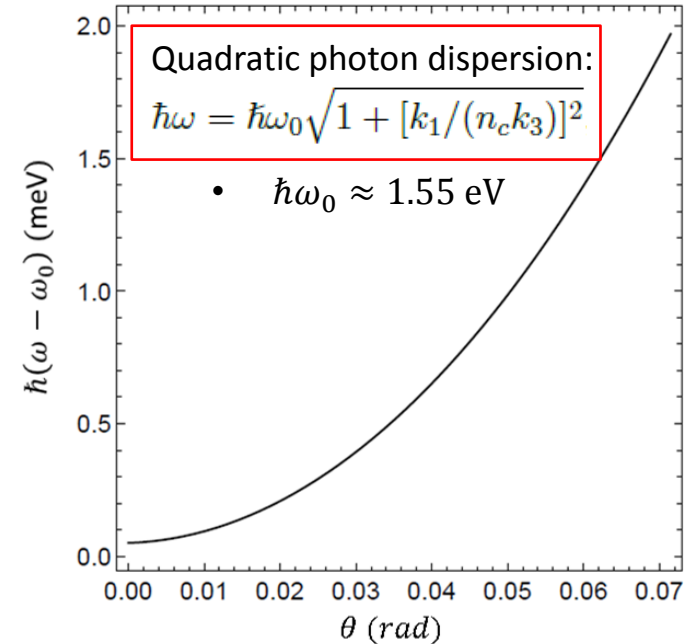


The planar optical microcavity model: results

This was observed for several q values....



and light incidence angles!

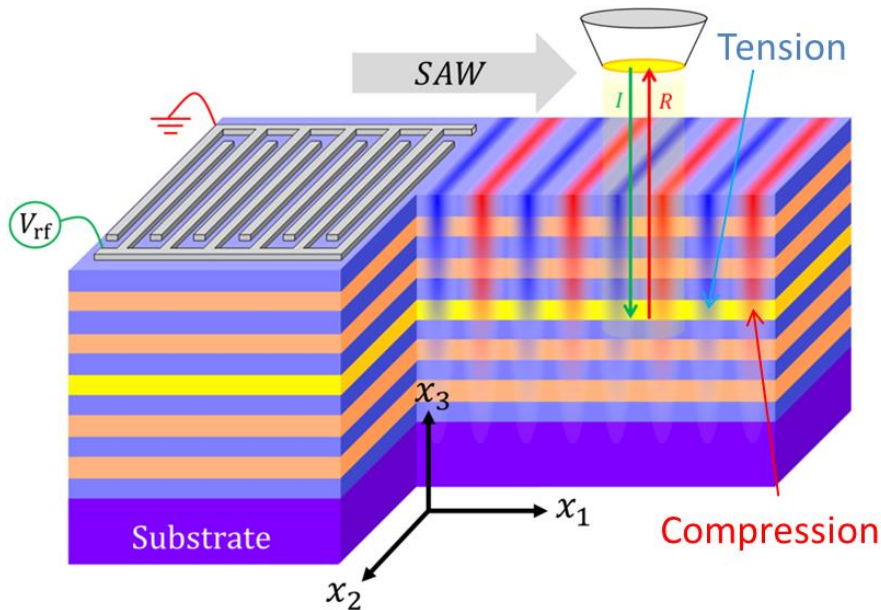


Using this model, we

- ✔ verified the unilateral optical confinement in the cavity
- ✔ characterized the reflectance and Q-factors for several q values (up to 10^4 for ~ 10 BMs)
 - good agreement with experimental results (ZnO/SiO₂)
- ✔ Constructed the photon dispersion for the POMC

The acousto-optic modulation model

Consider the following setup



SAW strain induces regions of tension and compression

The effective changes induced to the optical thickness of the cavity is given by*

$$\frac{\Delta\omega}{\omega} = - \left[\frac{\Delta n_c}{n_c} + \frac{\Delta d_c}{d_c} \right] = - \left[\frac{\Delta n_c}{n_c} + S_{33} \right]$$

Acousto-optic modulation

SAW-induced thickness modulation

$$n = \sqrt{\epsilon} \quad \longrightarrow$$

The dielectric modulation follows from the tensorial equation:

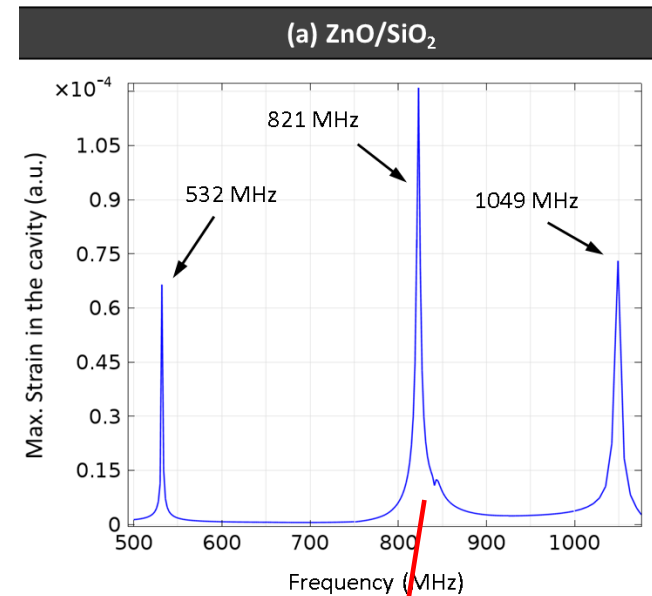
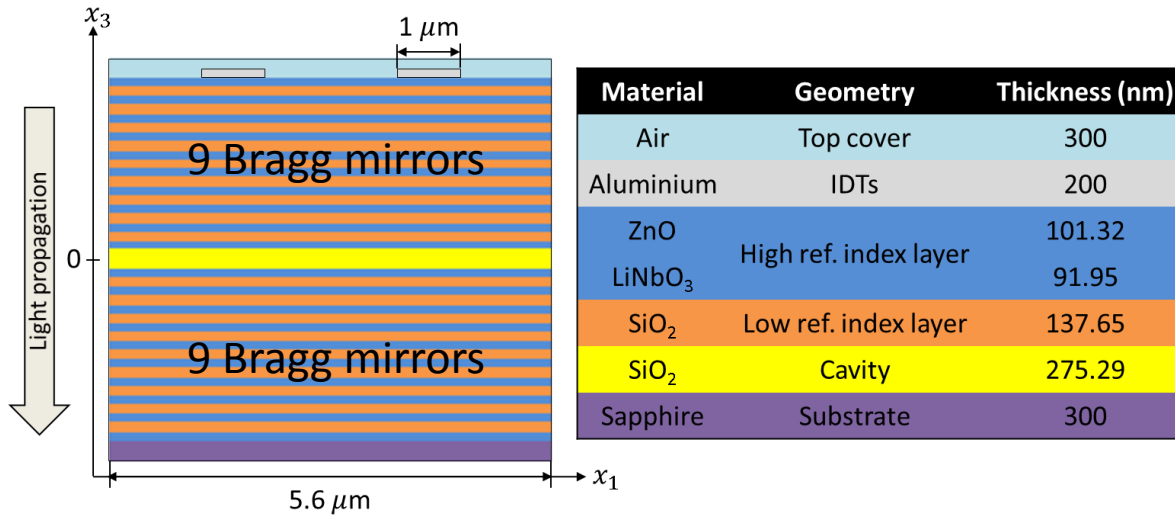
$$\Delta\epsilon_{il} = -\epsilon_{ij} p_{ijmn} \epsilon_{kl} S_{mn}$$

where p_{ijmn} is the acousto-optic tensor.

*M.M. de Lima et al. *Reports on Progress in Physics*, 68:1639, 2005.

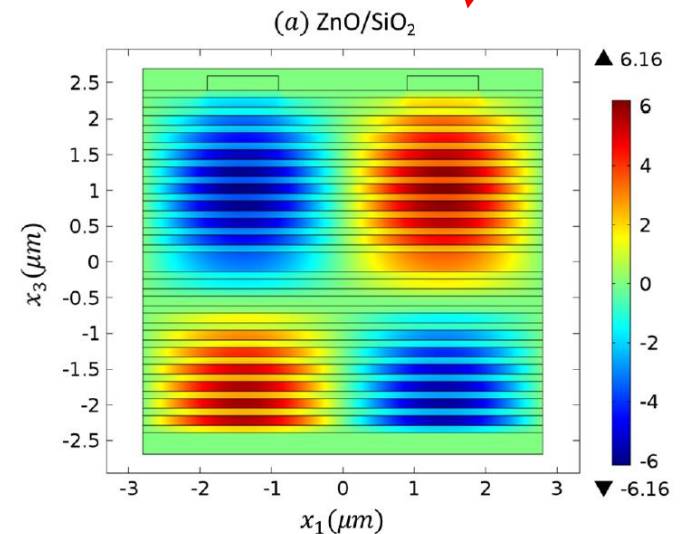
The acousto-optic modulation model

Solid Mechanics + Electromagnetic waves modules



- **Boundary conditions kept**
 - **Included a Sapphire substrate:**
 - Transparent
 - Hard
- Simulation steps:**
1. SAW modes evaluated
 - refractive index modulation
 2. Optical modes evaluated

$$\left(\frac{\Delta n}{n}\right)_3$$



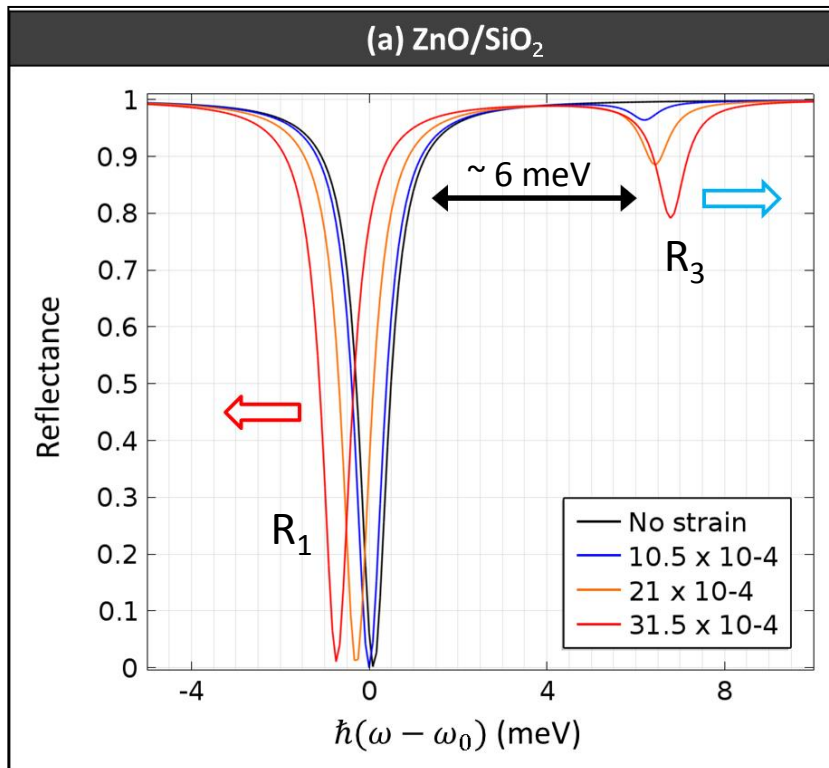
The acousto-optic modulation model: optical modes

Normal light incidence

As strain is increased

- 2 resonances appear
- R_1 redshifts
- R_3 blueshifts

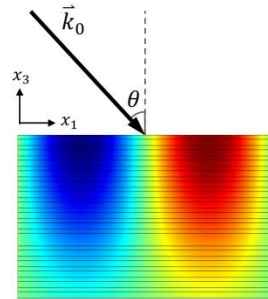
Near-resonance optical reflectance



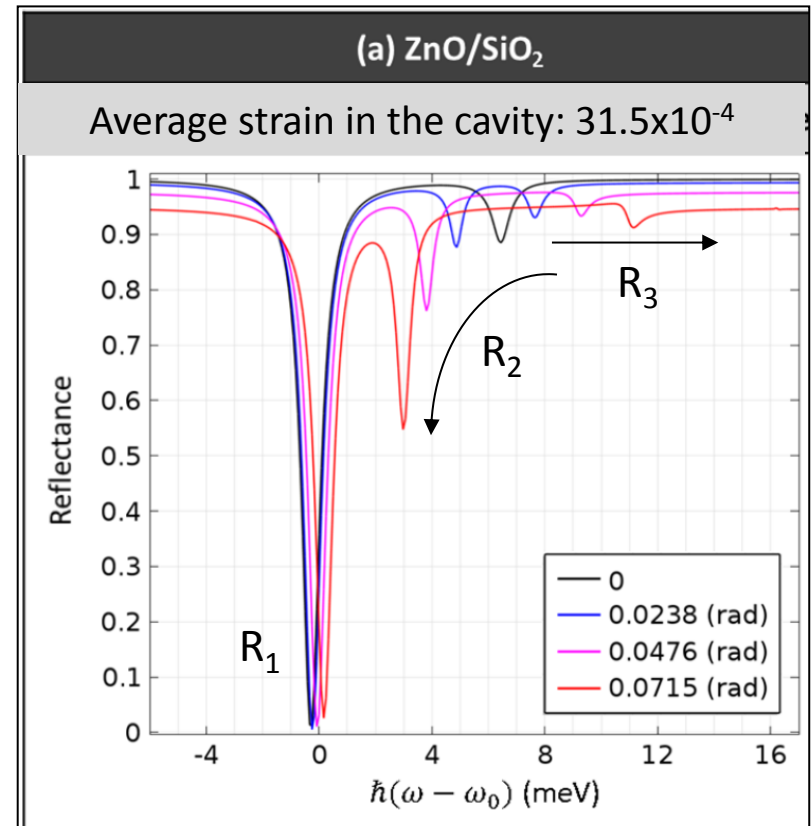
Oblique light incidence

As incidence angle increases

- 3 resonances appear
- R_2 redshifts



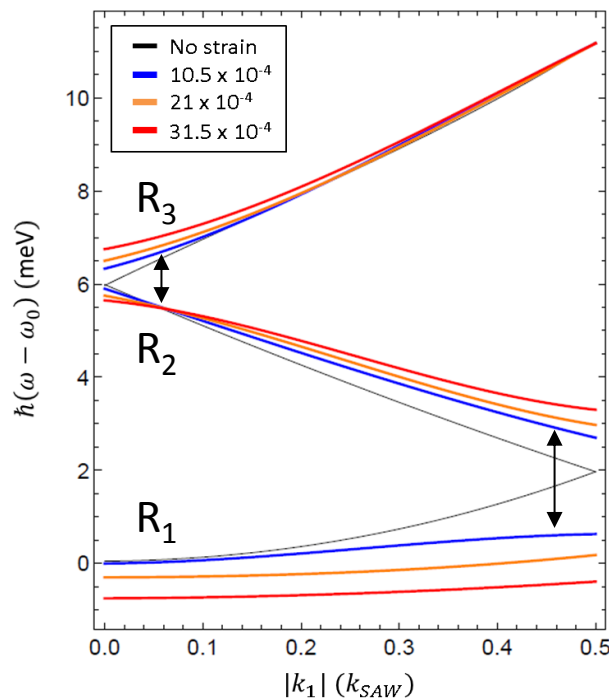
Near-resonance optical reflectance



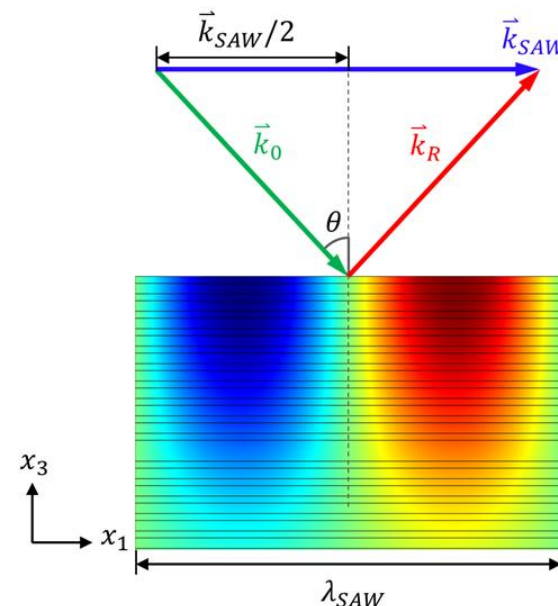
The acousto-optic modulation model: optical modes

When the SAW is turned ON

- SAW strains \Rightarrow **dynamic optical superlattice**
- Periodicity along x_1 is thus created, diffracting incoming light beams
- Photon dispersion is **folded into a mini Brillouin zone** (MBZ) between $k_1 \in [-k_{SAW}/2, k_{SAW}/2]$
- Increase of strain strengthens the phonon-photon interaction \Rightarrow **Energy gaps open up**



$$\theta_{max} = \text{Sin}^{-1}\left(\frac{k_{SAW}}{2k_0}\right) \approx 0.0715 \text{ rad}$$



Conclusions

Acoustic model

- Prediction of SAW resonances
 - Good agreement with experimental results
- Mode characterization
- Sample engineering

Optics model

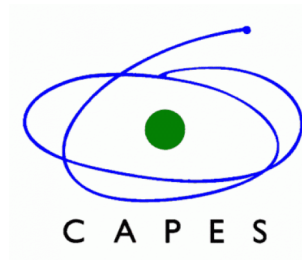
- Prediction of modes
- Light confinement observed
- Reflectance, Q-factors, dispersions characterized
- Good agreement with the TM method

SAW + POMC interaction

- Strong photon-phonon interaction
- Splitting and shifting of optical resonances
- Folding of photon dispersion
- Dynamic optical superlattice

Thank you for your attention!

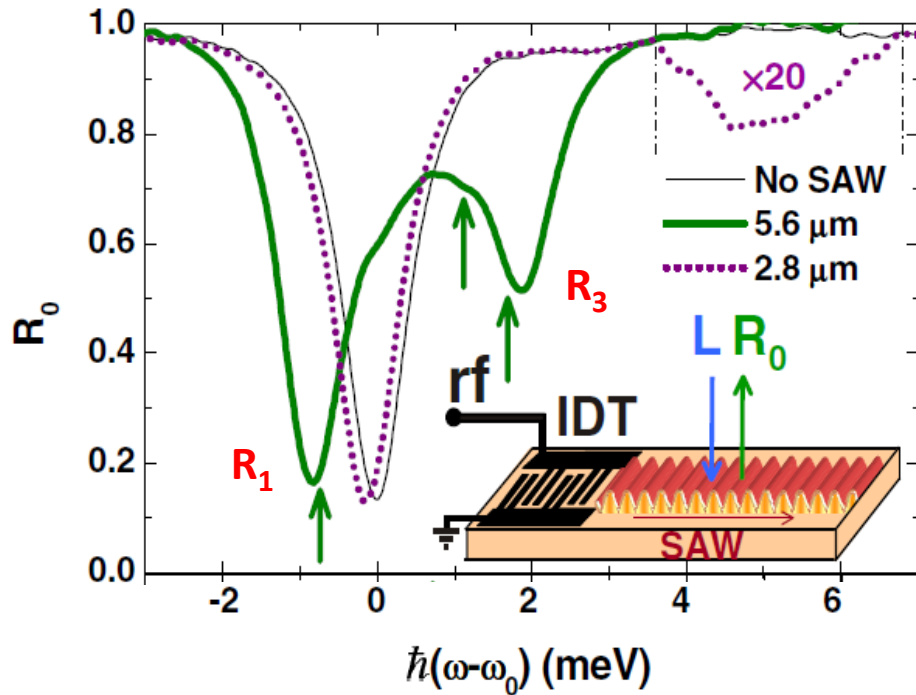
Acknowledgements



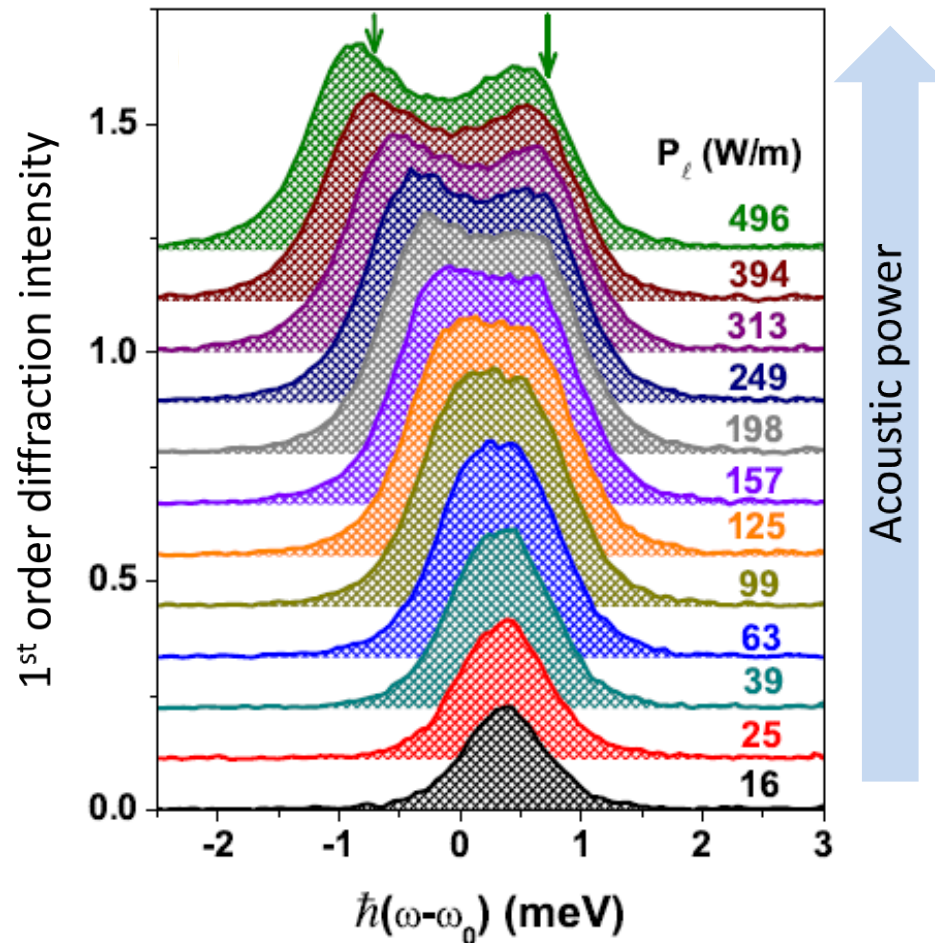
The acousto-optic modulation model: optical modes

Experimental reports on $\lambda/2$ GaAs/AlAs POMCs (Q = 1200)*

Normal incidence



$$\theta_{max} = \text{Sin}^{-1} \left(\frac{k_{SAW}}{2k_0} \right) \text{ (right border of the MBZ)}$$



- Two pronounced modes observed
- As we observed in our model

*M.M. de Lima et al. *Phys. Rev. Lett.*, 94:126805, 2005.