

Highest Pulsed Magnetic Fields in Science and Technology,



Hochfeld-
Magnetlabor
Dresden

Assisted by Advanced Finite-Element Simulations



Forschungszentrum
Dresden Rossendorf

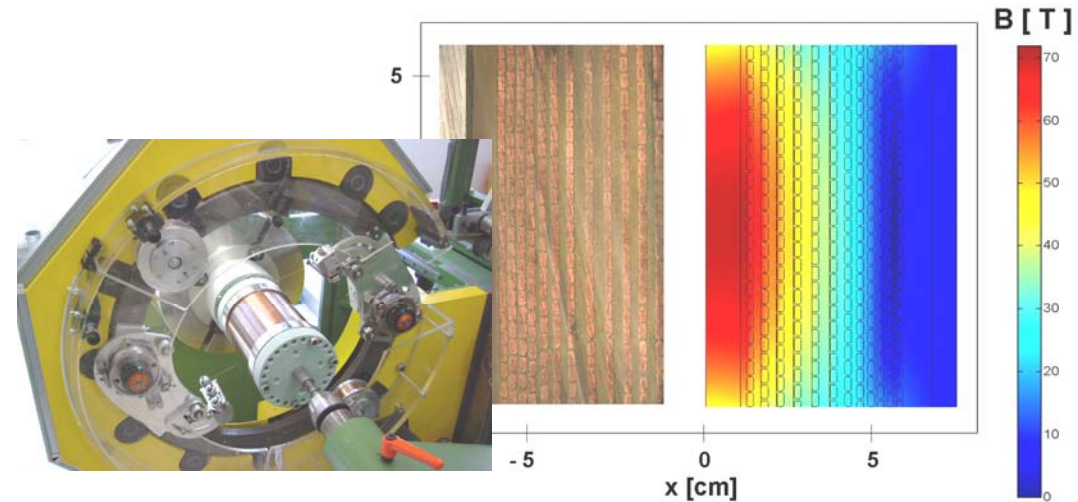
1) Highest magnetic fields for advanced materials studies



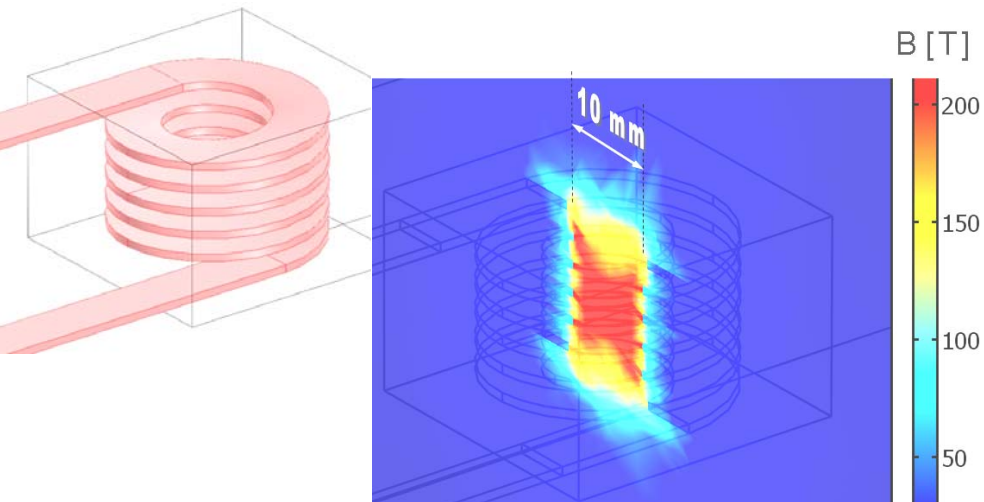
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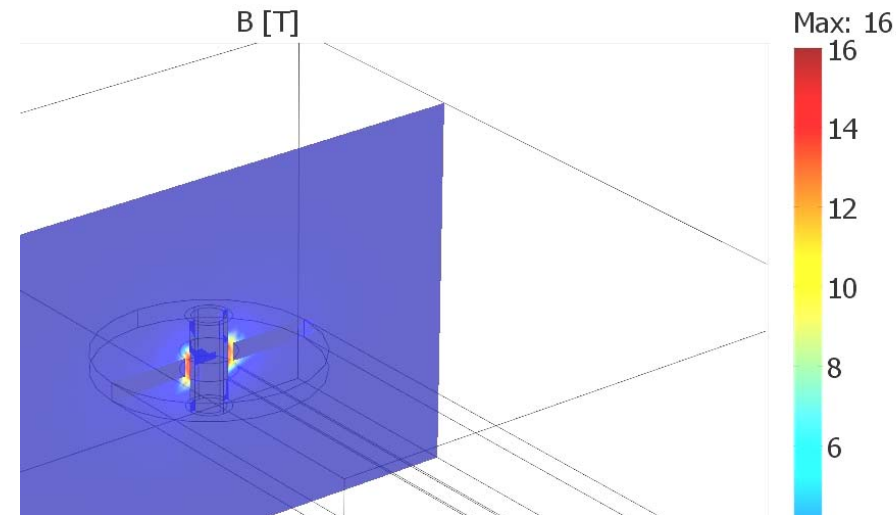
2) Design, fabrication, and use of pulsed-field coils for materials research

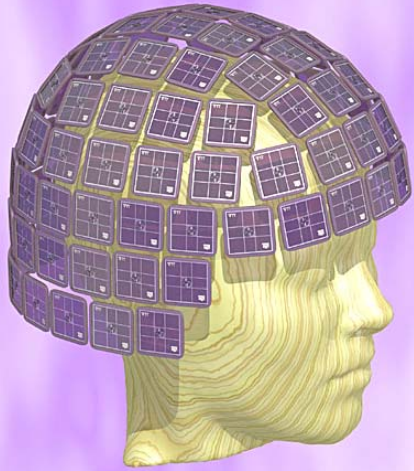


3) Simulation of pulsed-field coils for ultimate flux densities



4) Simulation of electromagnetic pulse-forming processes





Biology
pT – nT



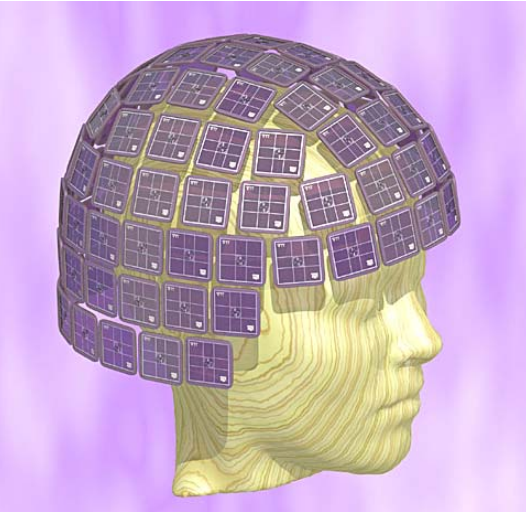
Civilization
~ μT



Earth
45 μT



Sun
0.1 T



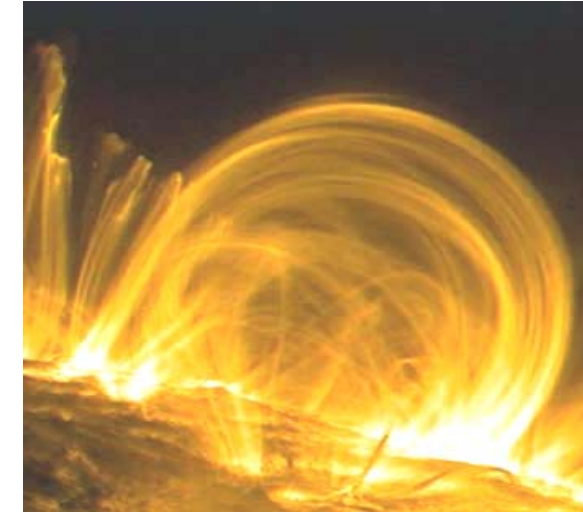
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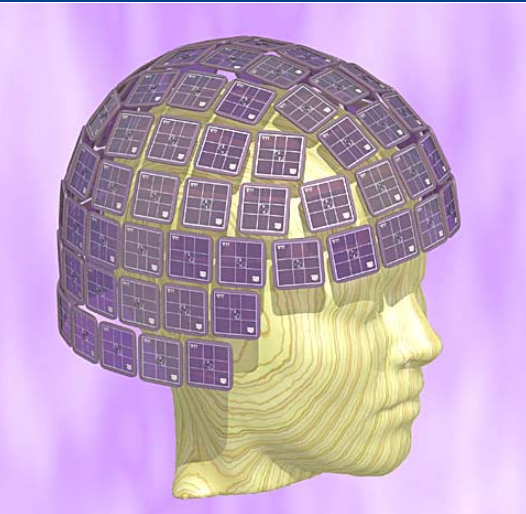
Earth
45 μT



Sun
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Diagnostics
~ 1 T



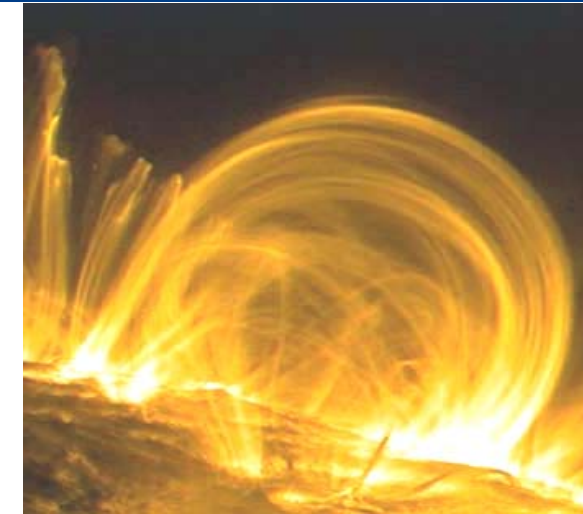
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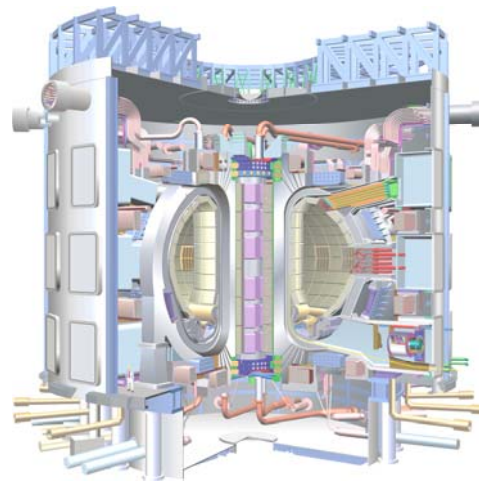
Earth
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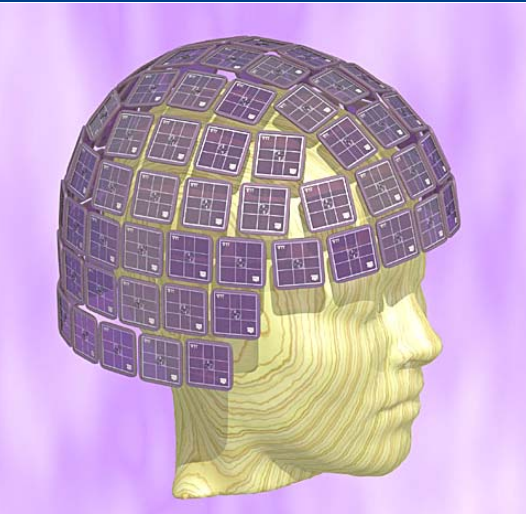
Sun
0.1 T



Diagnostics
~ 1 T



Fusion
~ 10 T



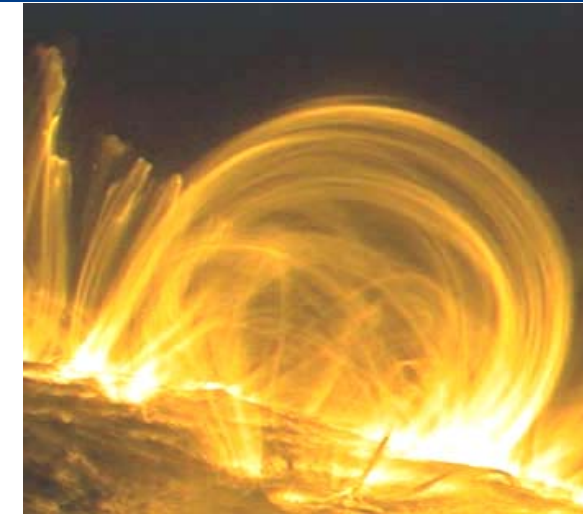
Biology
pT – nT



Civilization
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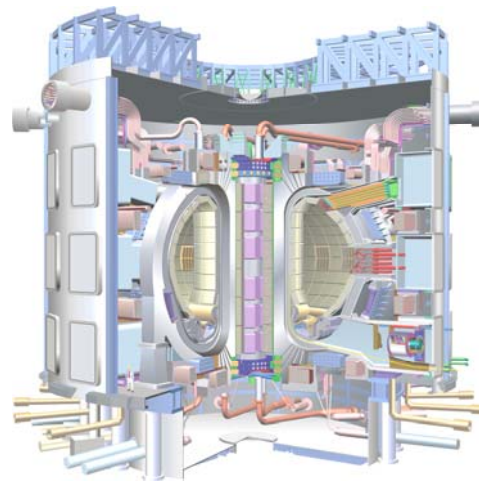
Earth
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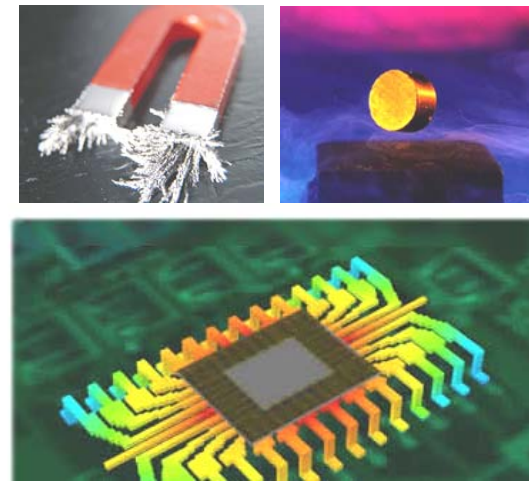
Sun
0.1 T



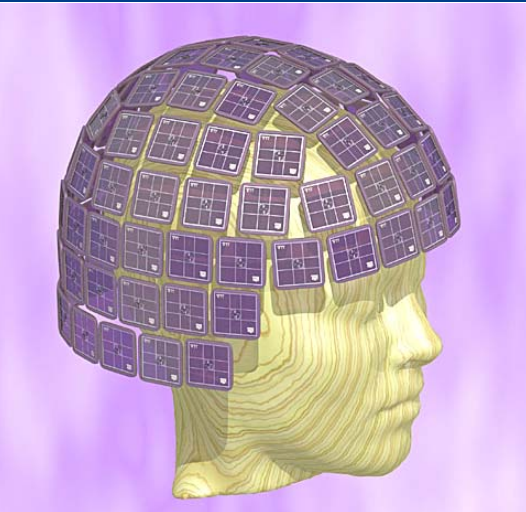
Diagnostics
~ 1 T



Fusion
~ 10 T



Materials
μT – 1000 T



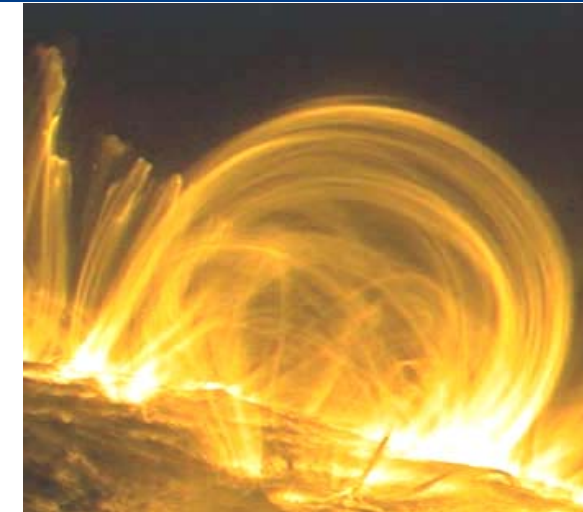
Biology
pT – nT



Civilization
~ μT



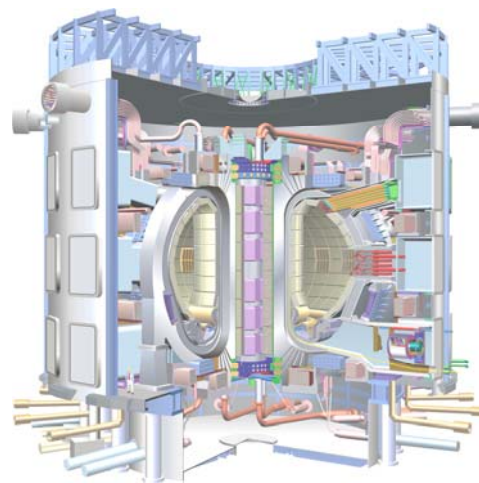
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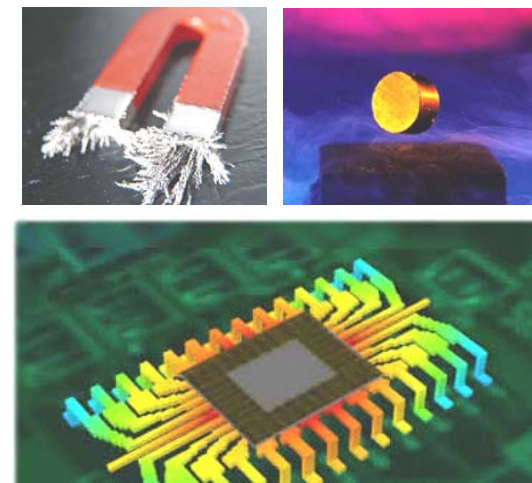
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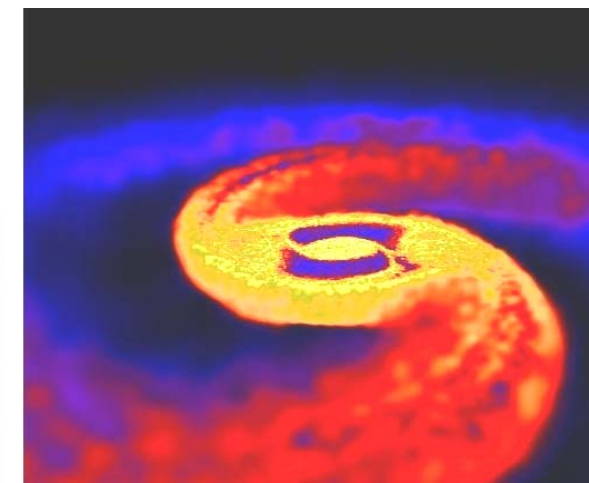
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Materials
μT – 1000 T

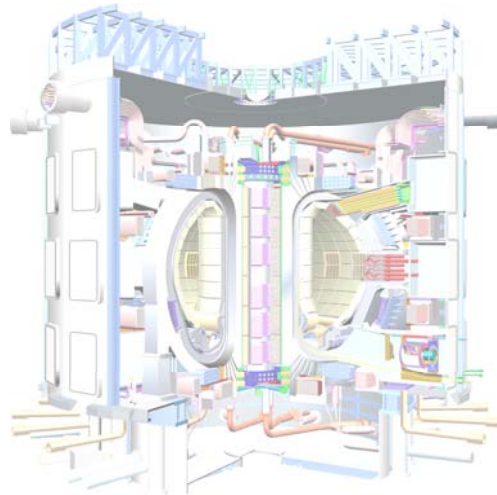


Neutron stars
10⁸ – 10¹¹ T



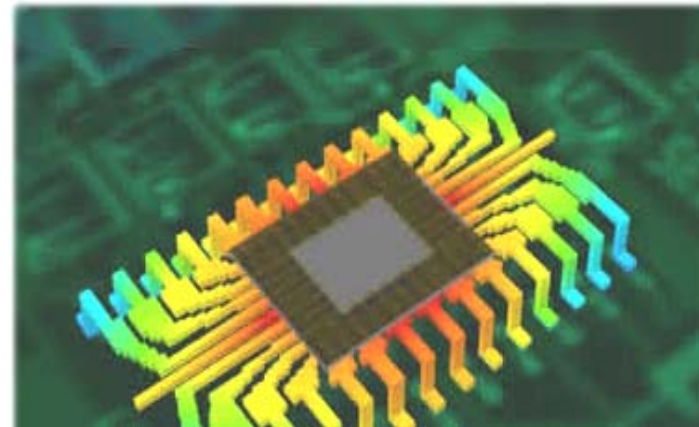
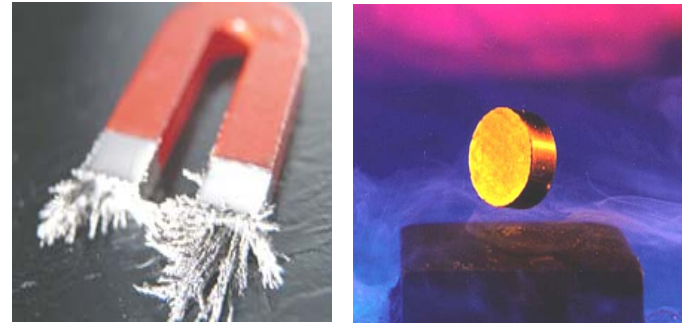
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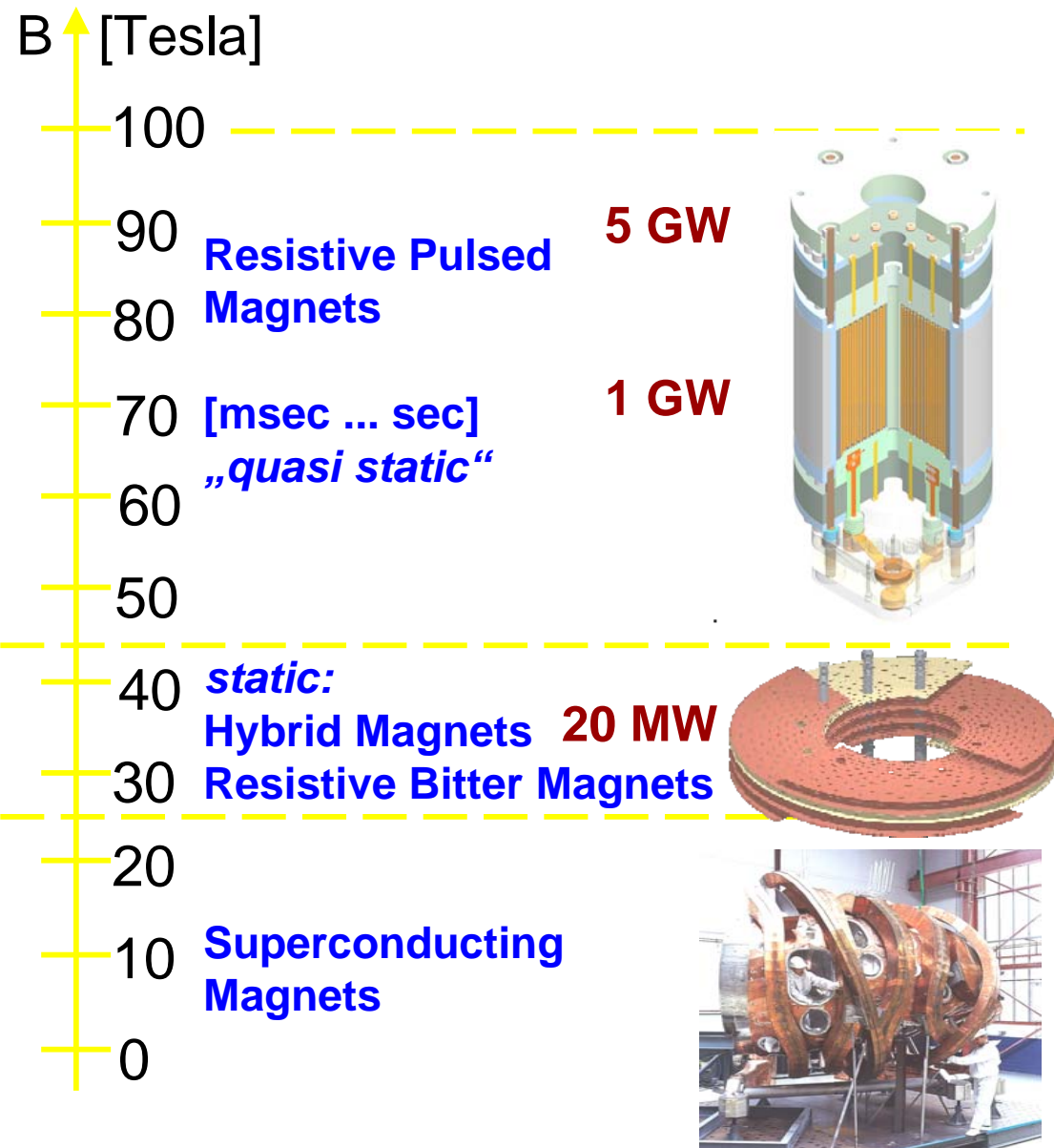
Materials

$\mu\text{T} - 1000 \text{ T}$

- Ferromagnets
- Antiferromagnets
- Multiferroics
- Strongly correlated electron systems
- Superconductors
- Semiconductors
- Nanoclusters
- Low-D spin systems
- Metal organics
- Proteins
- ...

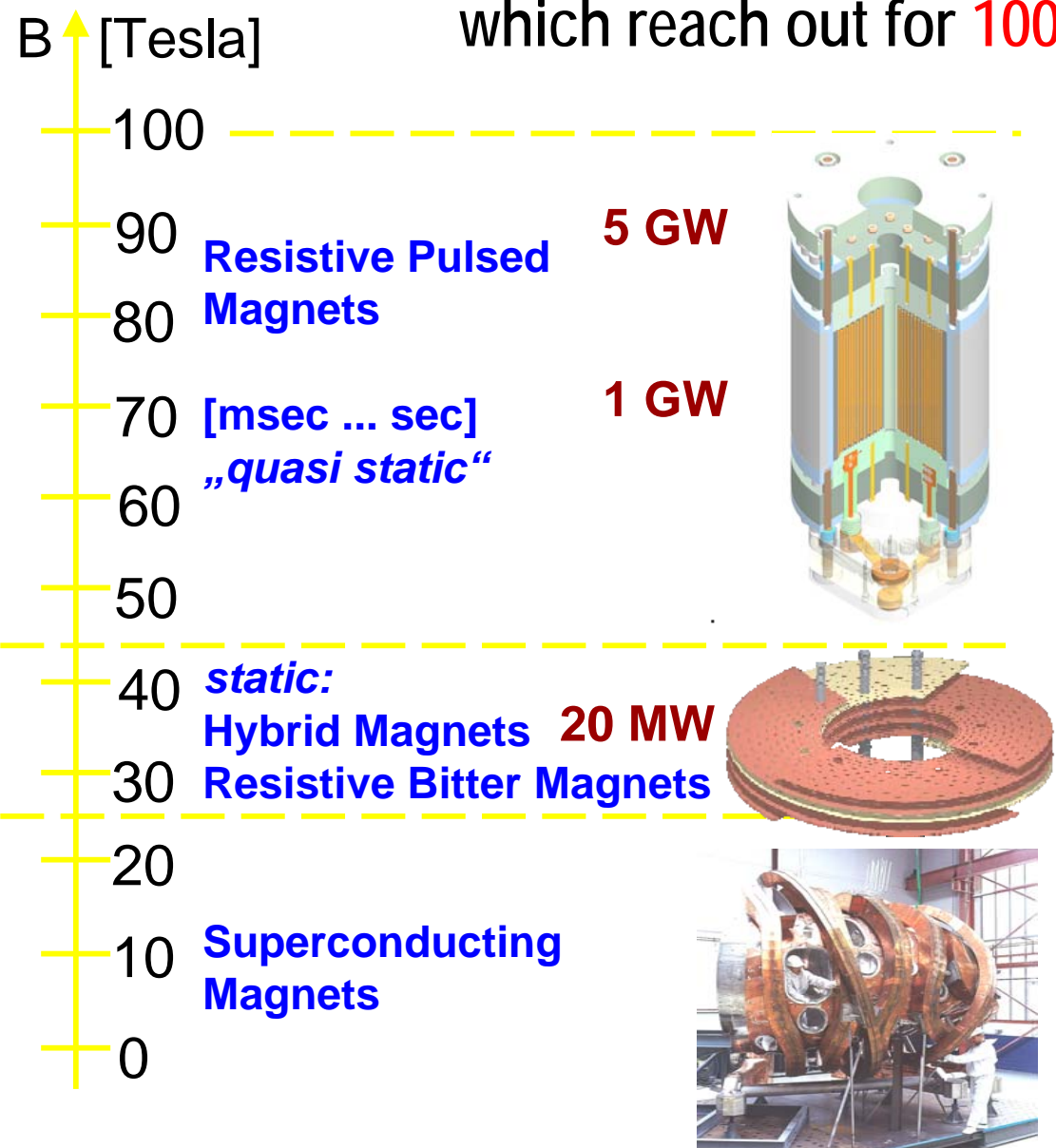
+Research on advanced techniques in pulsed magnetic fields

1) Highest magnetic fields for advanced materials studies



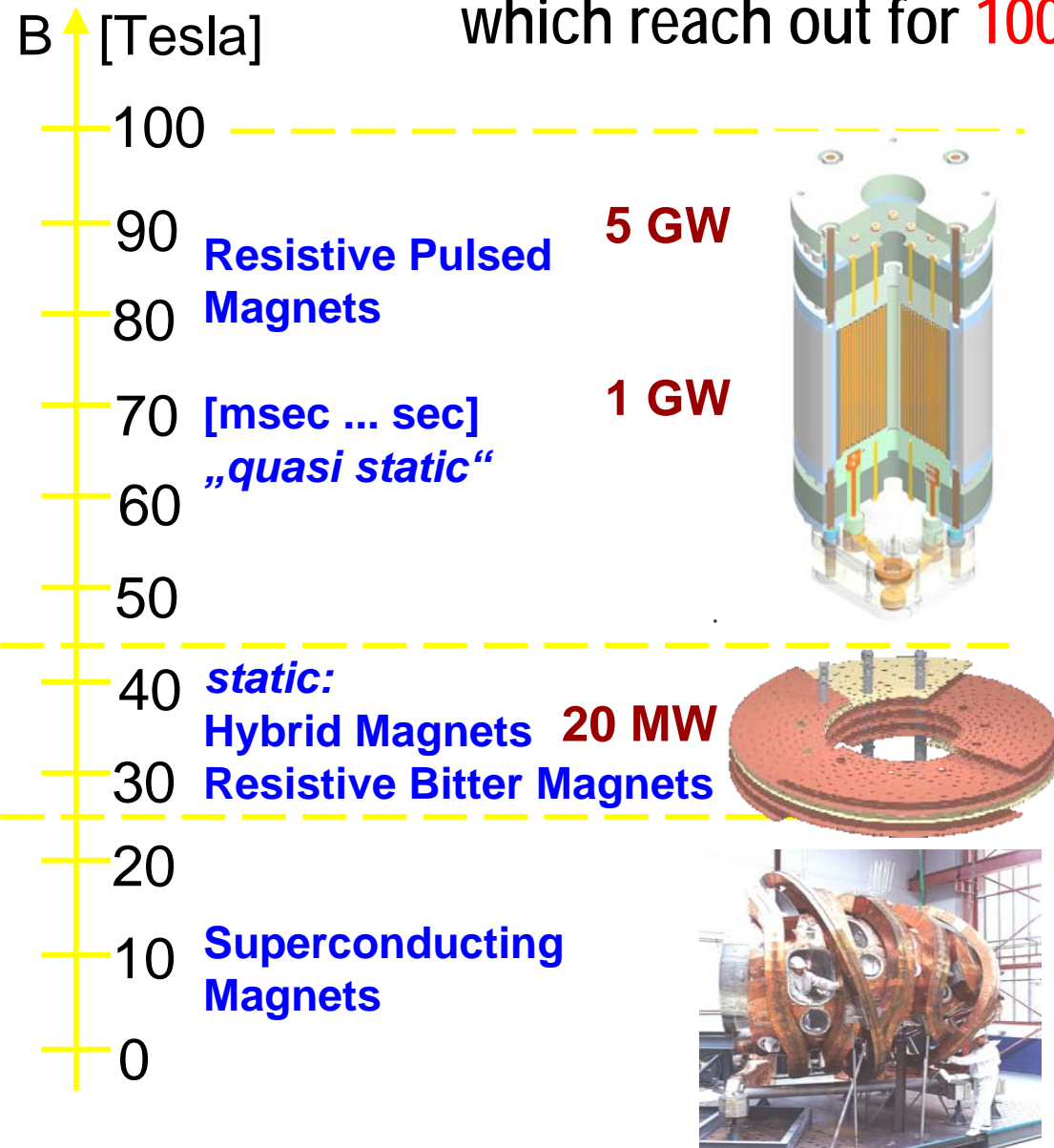
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HLD is one of the three user facilities (**Los Alamos, Dresden, Tokyo**) which reach out for **100 T** for research on advanced materials



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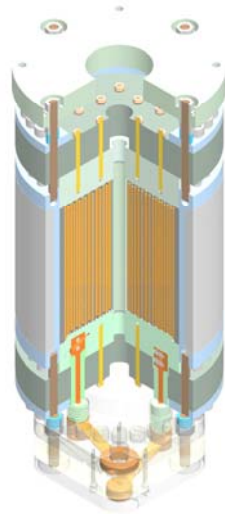
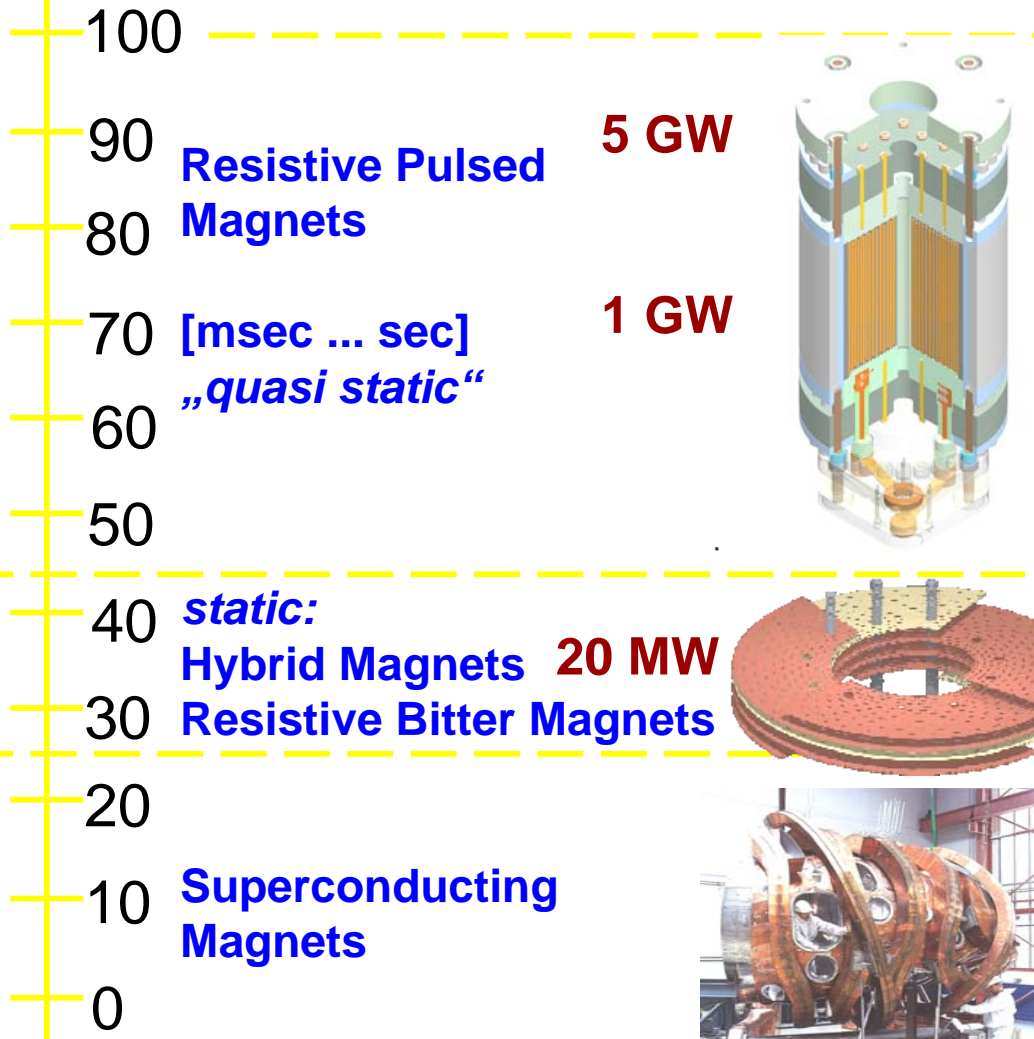



The Quest for 100 T in the quasistatic (0.01 ...1 sec) time range

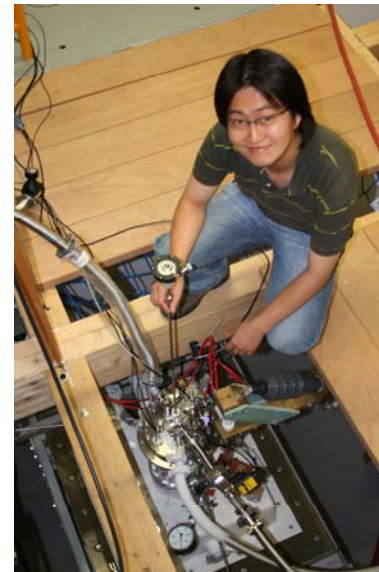
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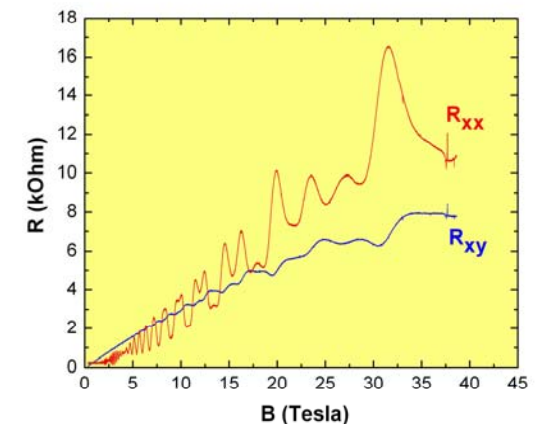
B [Tesla]



- HLD was evaluated and recommended by the German Science Council
- HLD is worldwide the only facility which provides combined access to high magnetic fields and intense IR-FIR radiation
- HLD is financed by  Bundesministerium für Bildung und Forschung 



„advanced materials in high magnetic fields“



$$B \sim \mu_0 N I / l$$

$$B = 50 \dots 100 \text{ T,}$$

$$\text{Current } I \sim 100 \text{ kA}$$

50 MJ / 24 kV / 600 kA / 5 GW modular capacitive pulsed-power supply

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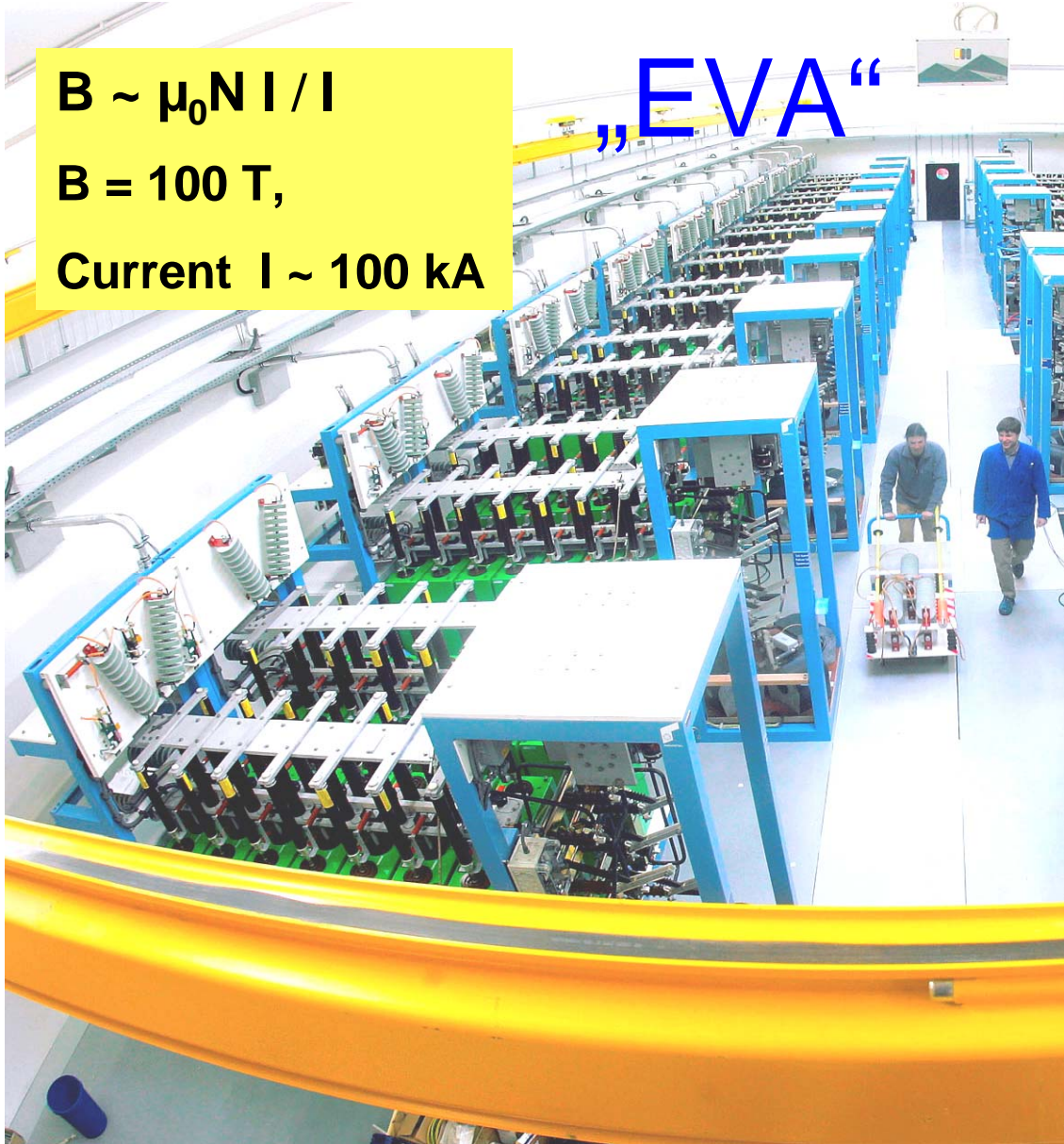
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50 MJ:

18 000 kg at 270 km/h



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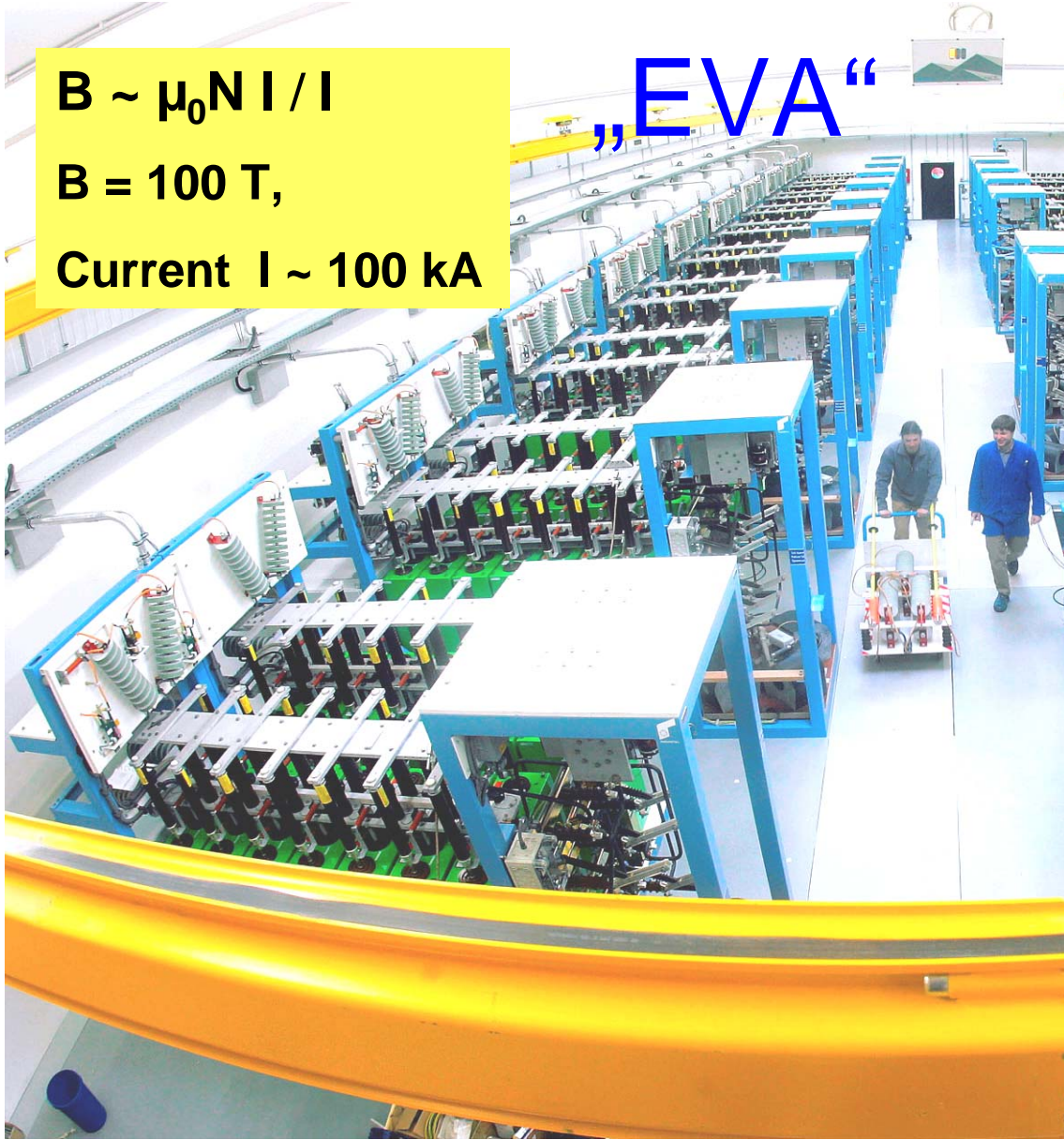
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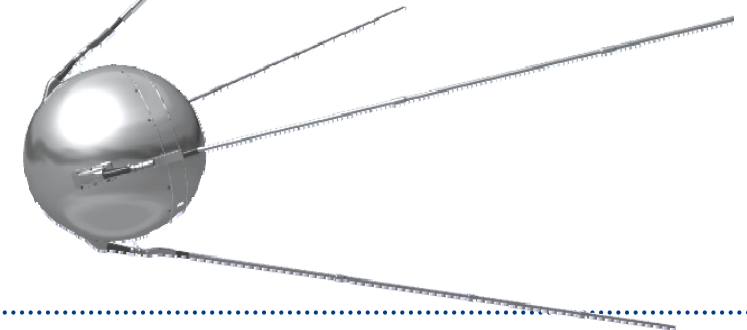


50 MJ:

18 000 kg at 270 km/h



1.8 kg at 27.000 km/h



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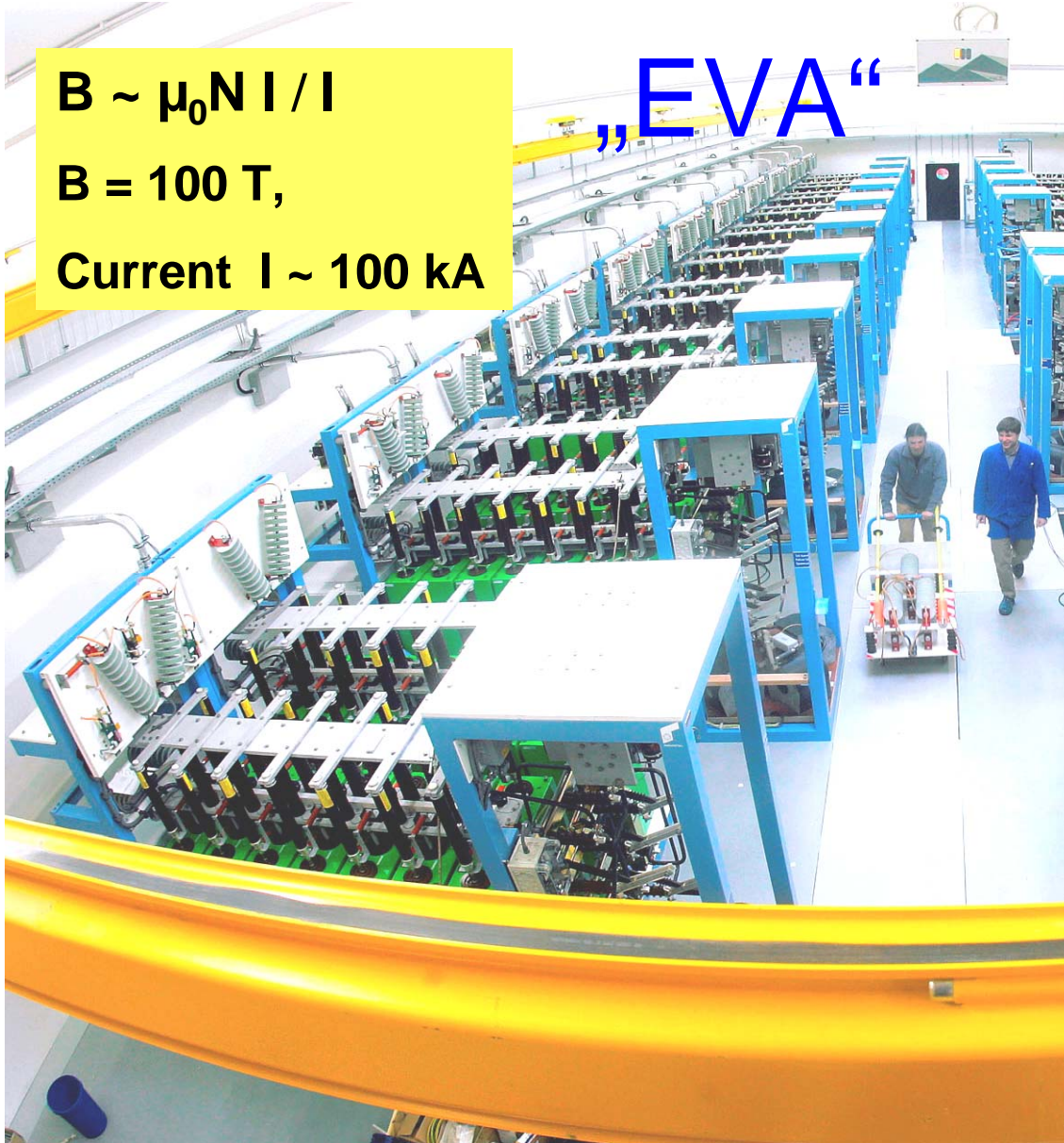
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5 GW ~ 7.000.000 Ps

~ power production/ consumption of a few million people



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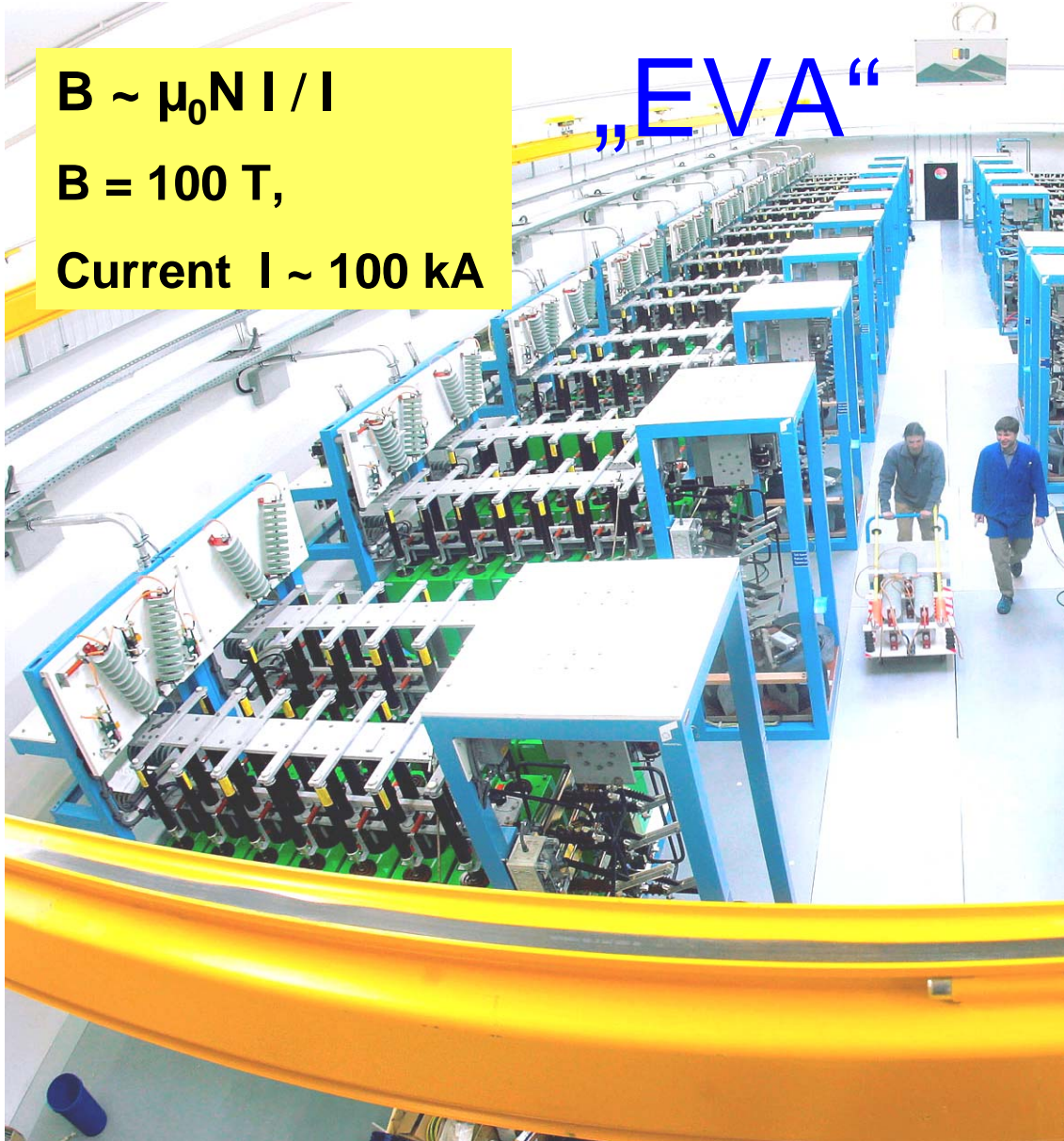
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5 GW ~ 7.000.000 Ps

~ power production/ consumption of a few million people

~ or: power of a rocket



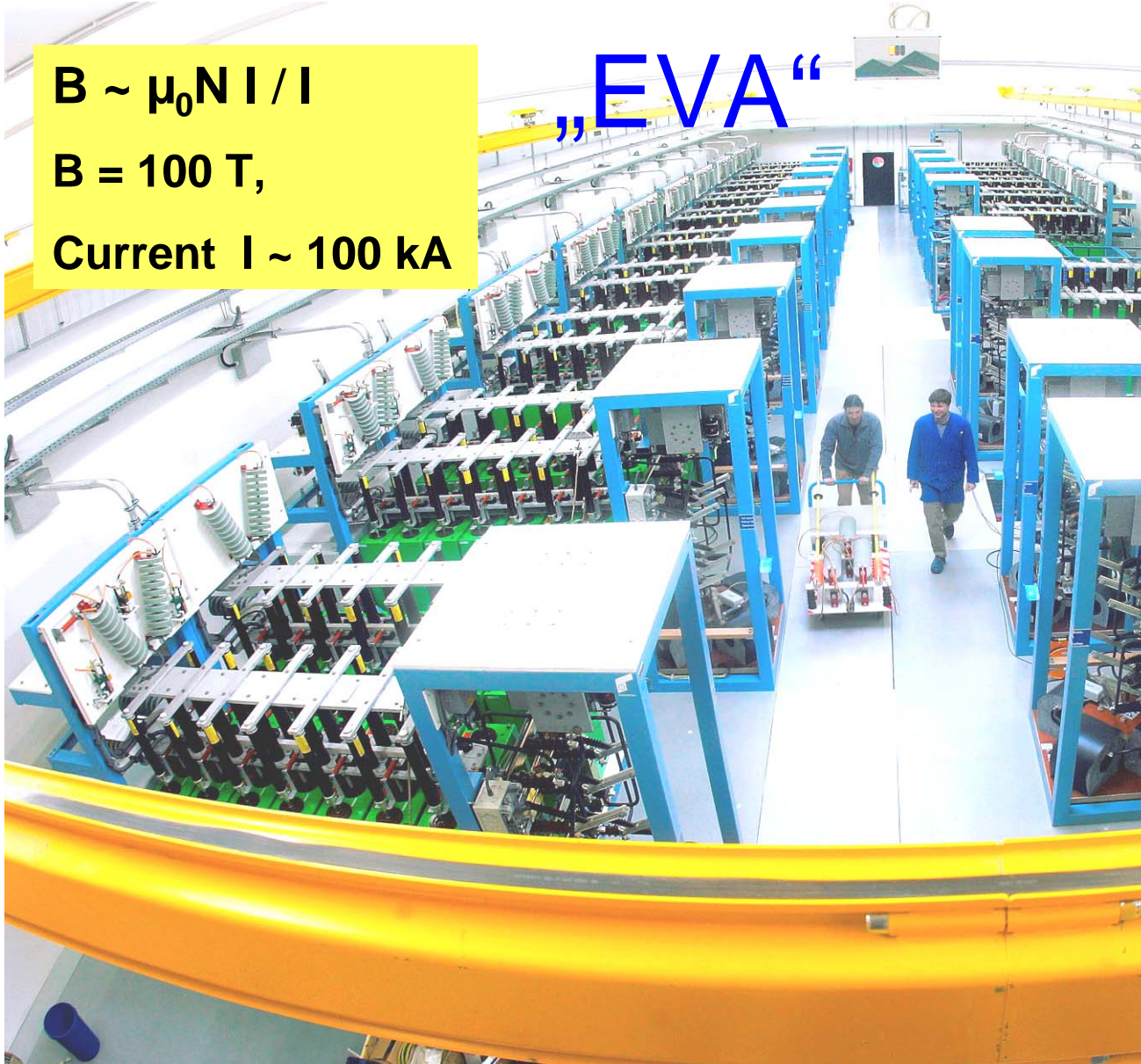
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22nd Feb. 2006

Costs of 50 MJ ?



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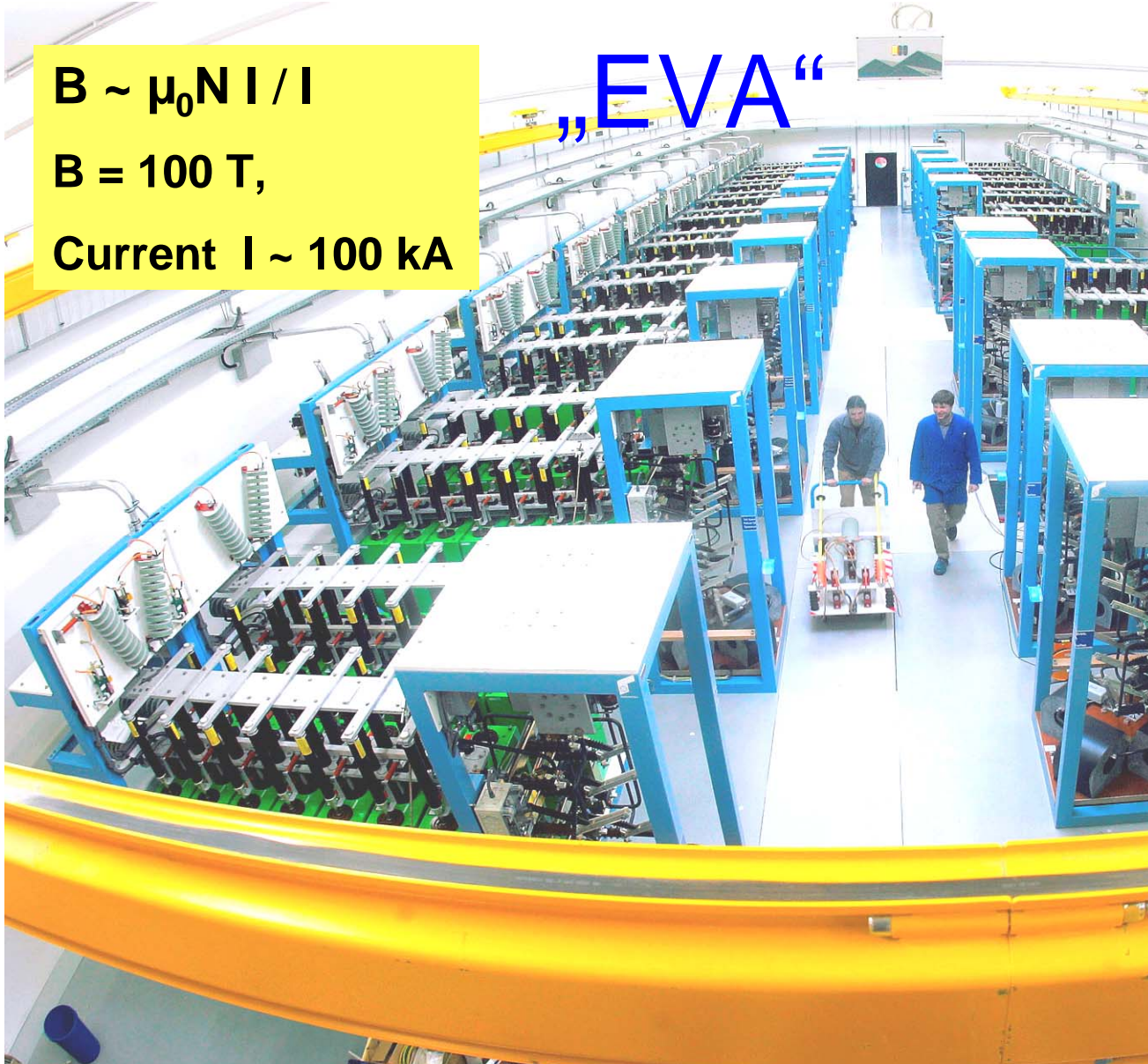
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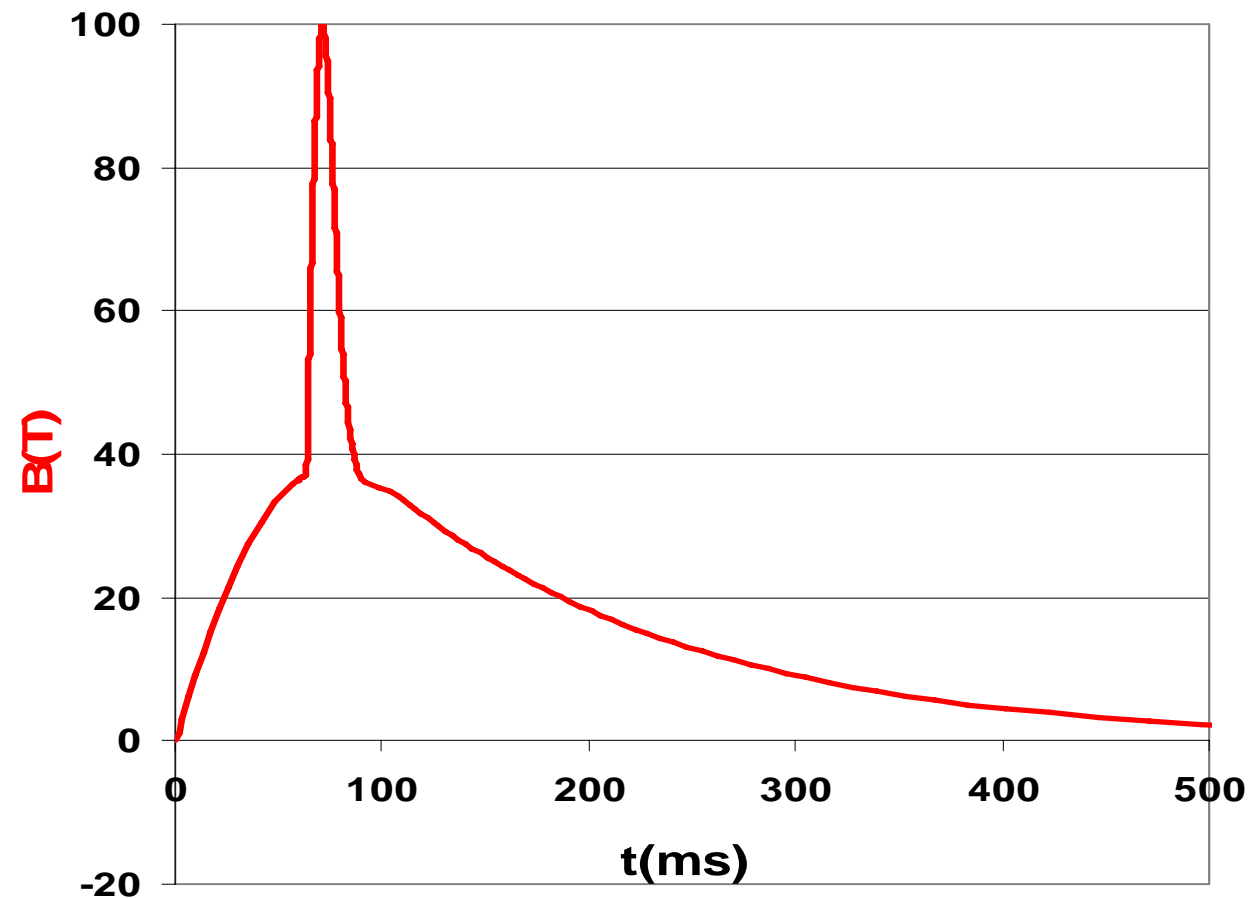
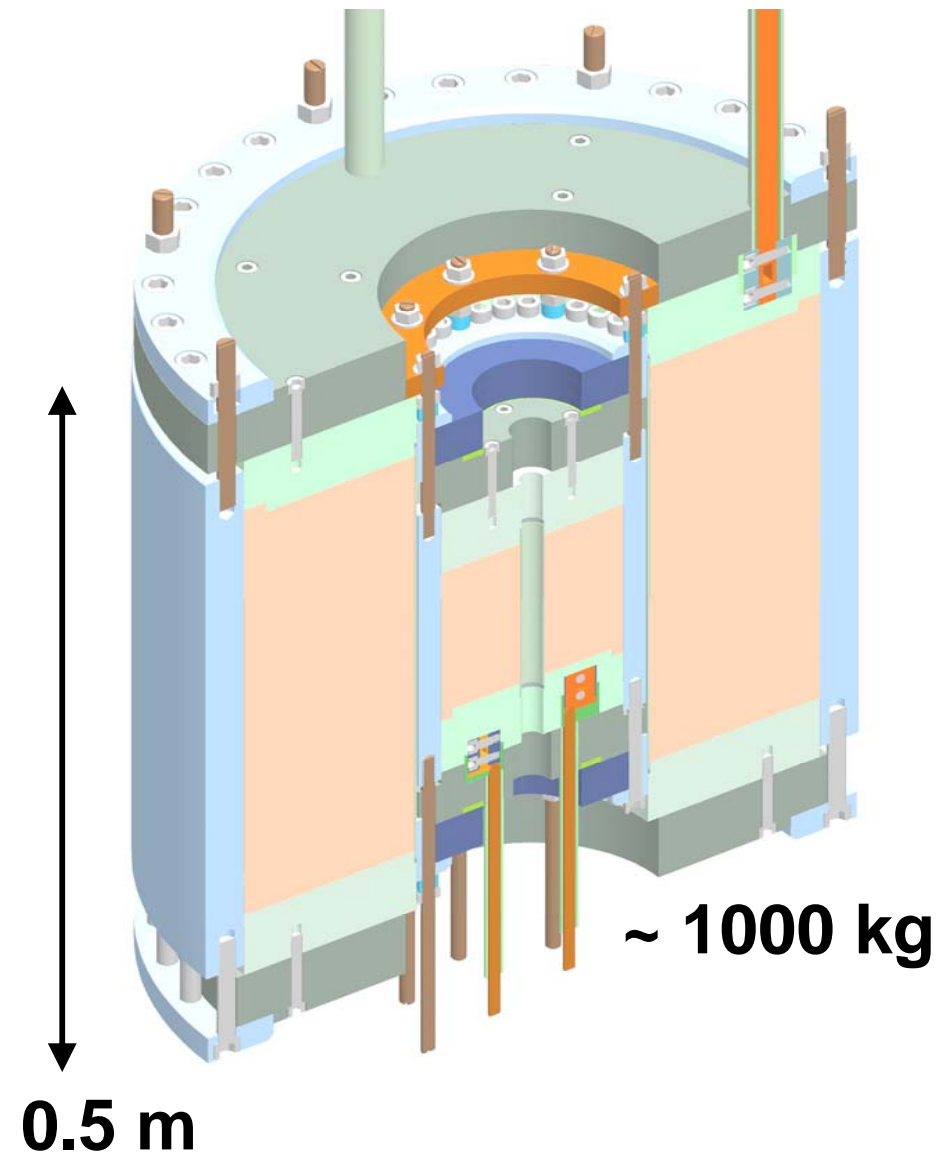
22nd Feb. 2006

Costs of 50 MJ ?



~ 2 €!

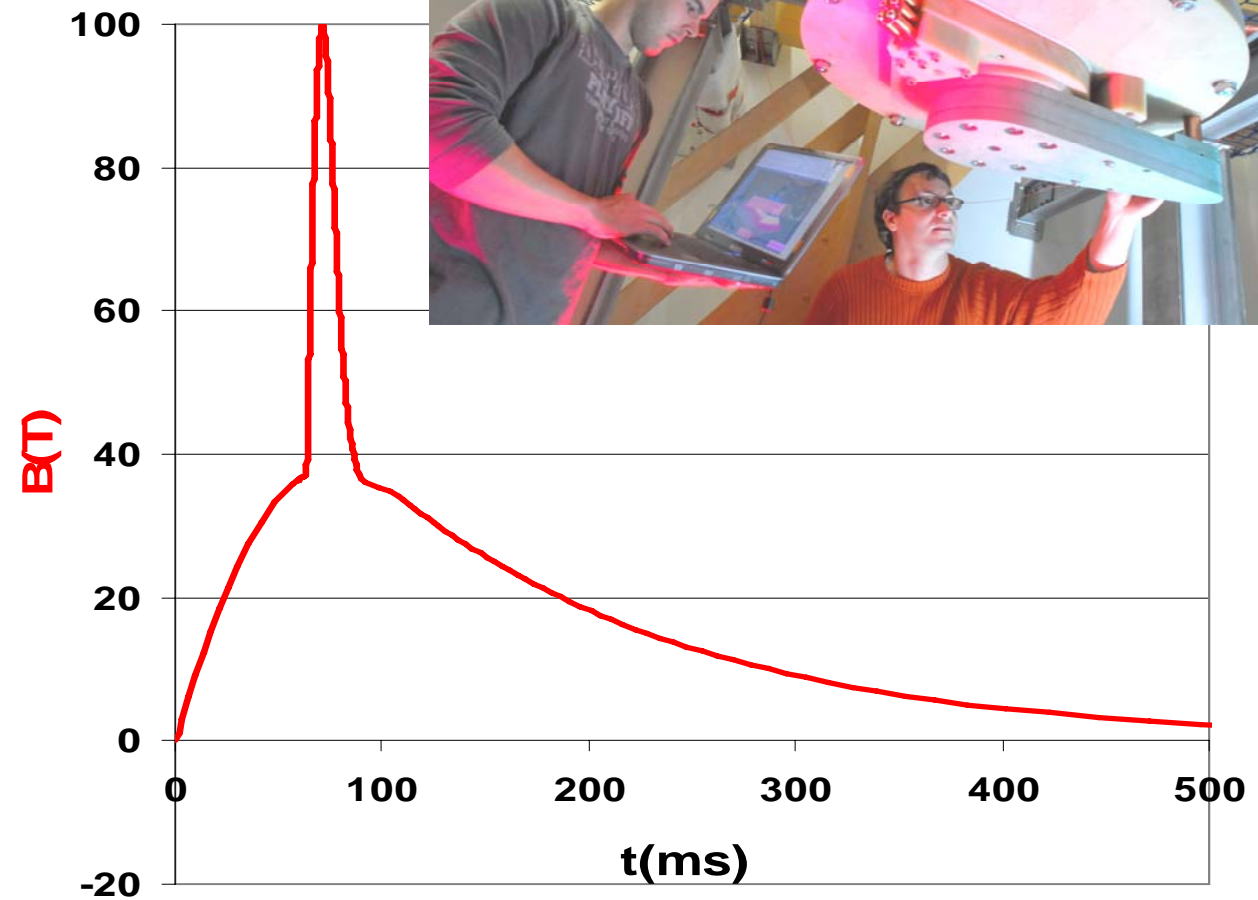
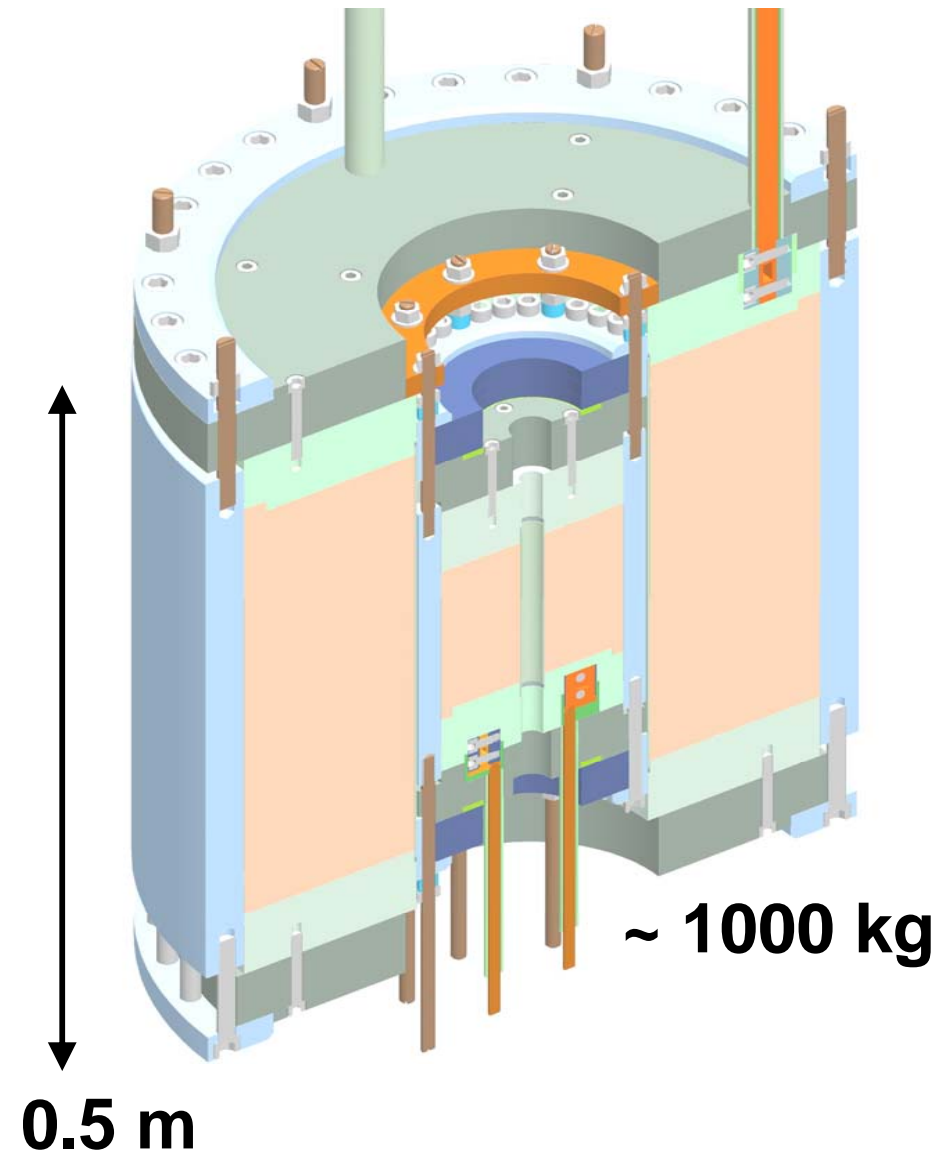
100 T double coil magnet (43 MJ / 3 MJ)



Inner: 20 mm bore, 10 layers CuNb 4x6 mm²

Outer: 10 layers Cu 8x14 mm²

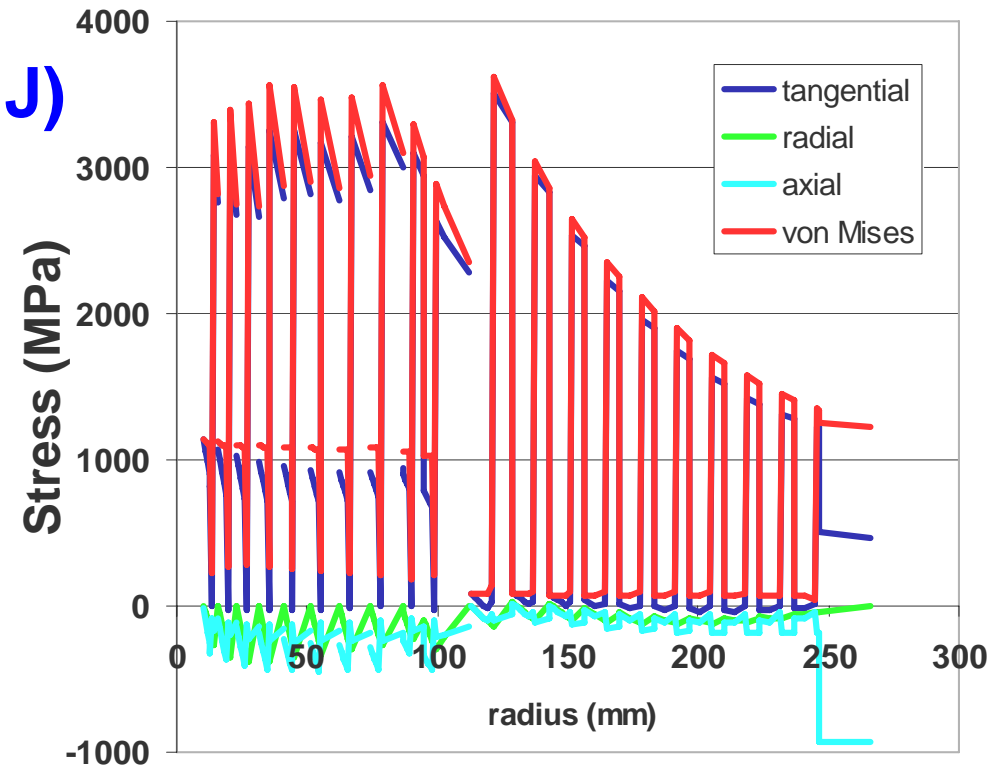
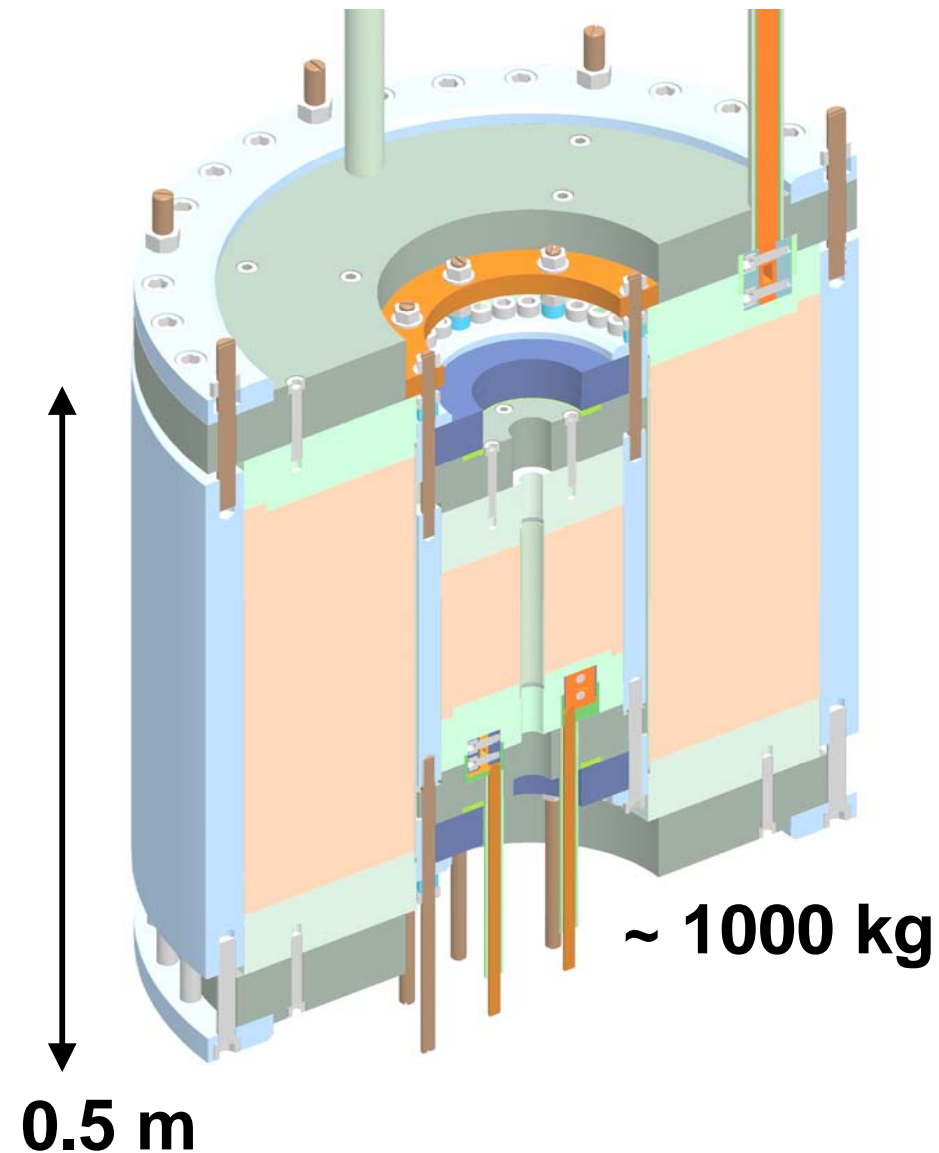
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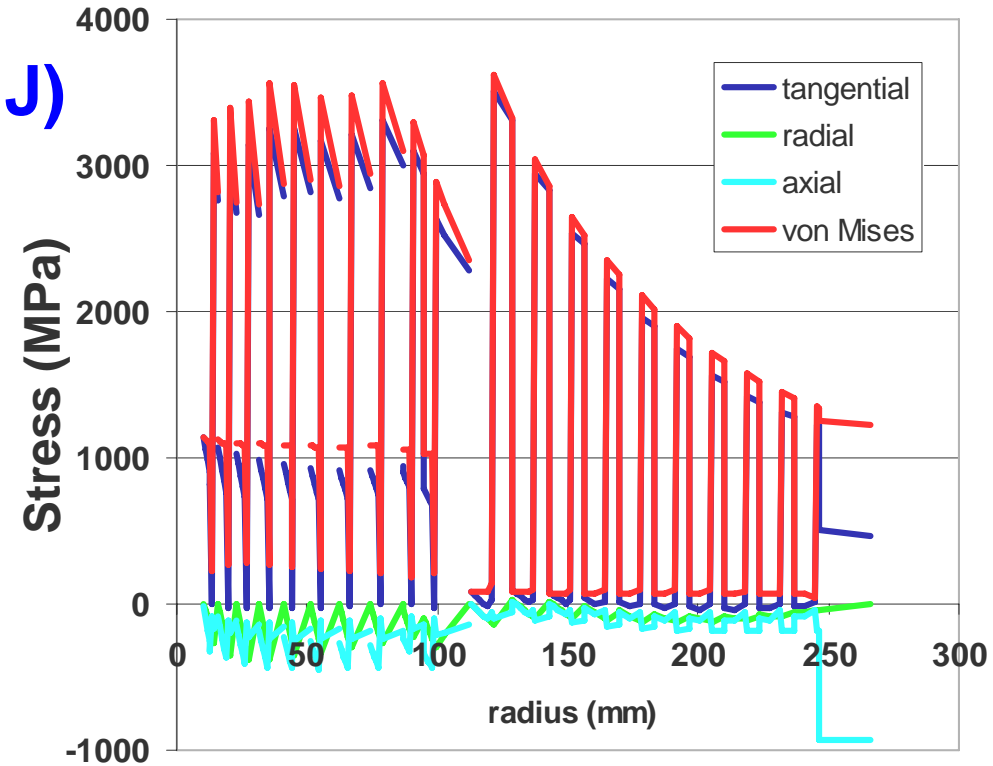
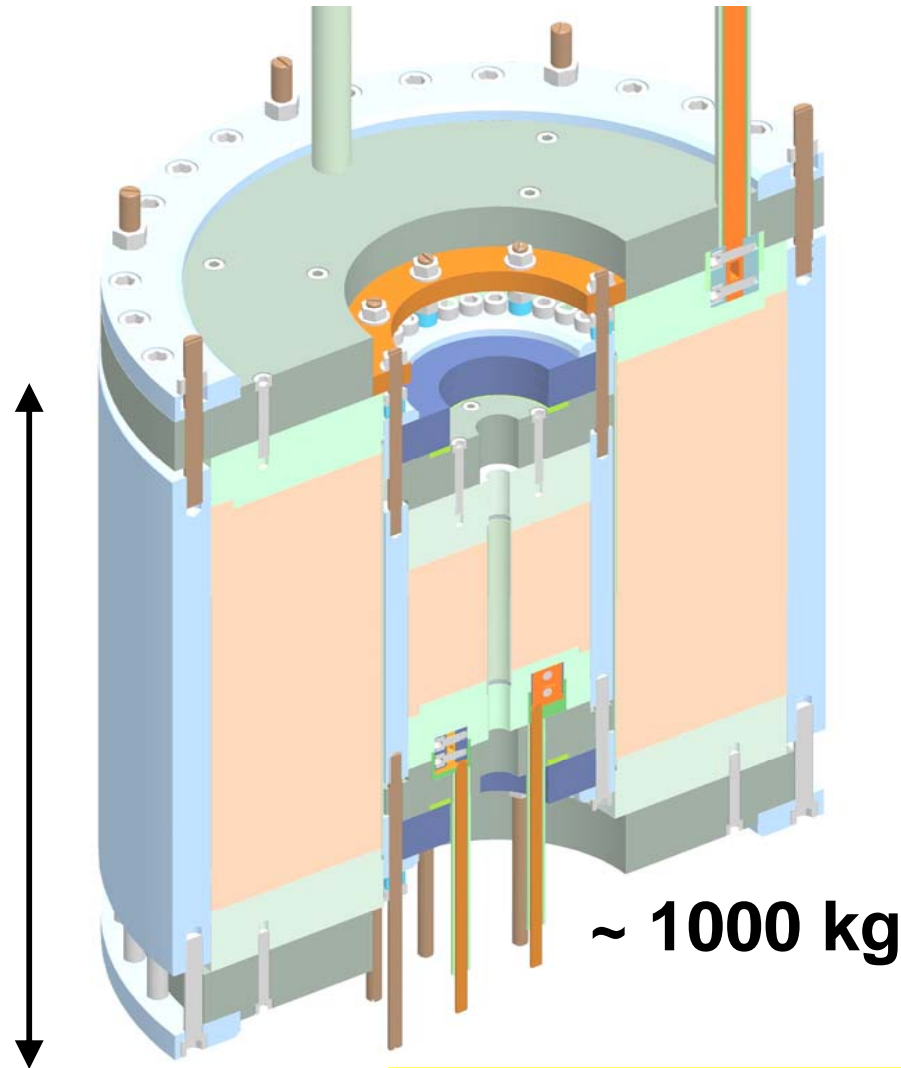
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Voltage: 10 ... 30 kV (short pulse!)

Heat up: 77 K → 350 K in msec

Stress: $P = B^2/2\mu_0 \sim 4 \text{ GPa}$ at 100 T

0.5 m

⇒ Realistic Multi-Physics FEM Simulation is needed!

a) Simple estimates ... give limits:

$$P = B^2/2\mu_0$$

$B = 50\text{T}$, $P \sim 1.0\text{ GPa}$ = upper limit of ultimate tensile strength of most steels

$B = 100\text{T}$, $P \sim 4.0\text{ GPa}$ = limit of ultimate tensile strength of fibre reinforcement

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b) Analytical solution using Biot-Savart law

- allows for precise and fast computation,

... but requires complex analytical solutions in restricted geometry segments

(see e.g.: L. Urankar et al., IEEE Transactions)

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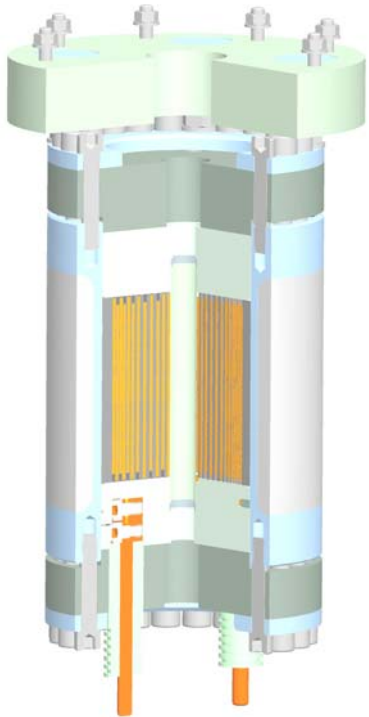
c) Numerical approach using **Finite-Element Analysis (FEA)**

- solves coupled partial differential equations under boundary conditions

- no restrictions in geometry, allows for multiphysical solutions ... but requires a considerable amount of computation time: fast solvers are needed

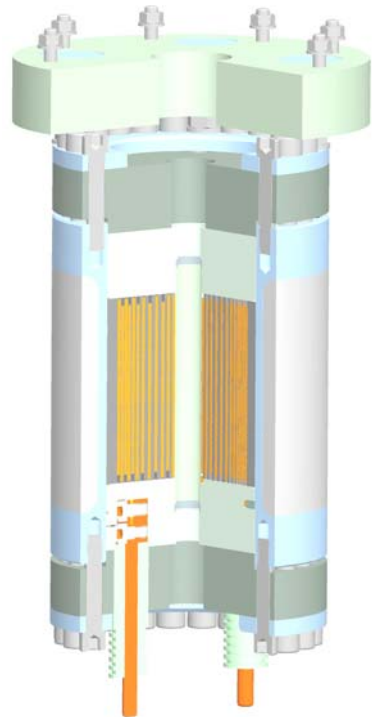
Multiphysics FEA via COMSOL

FEA example 1 (azimuthal symmetry):



300 turns, 12 layers, 3 mH,
 $t_{\text{Pulse}} = 100 \text{ msec}$

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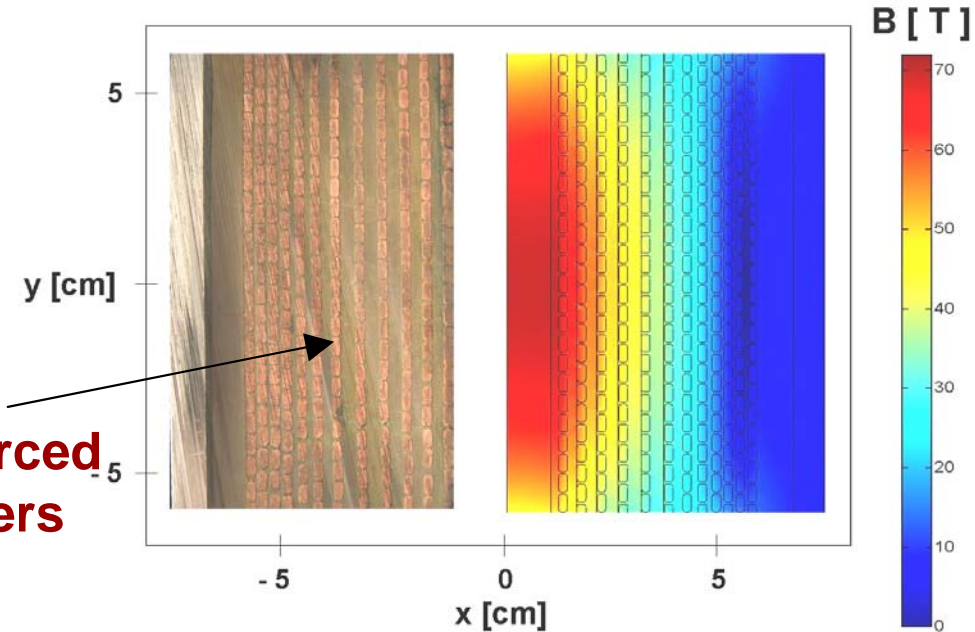


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FEA allows for calculation of, e.g.:

$B(x, y, z, t)$ up to 72 T

**Wires
reinforced
by fibers**

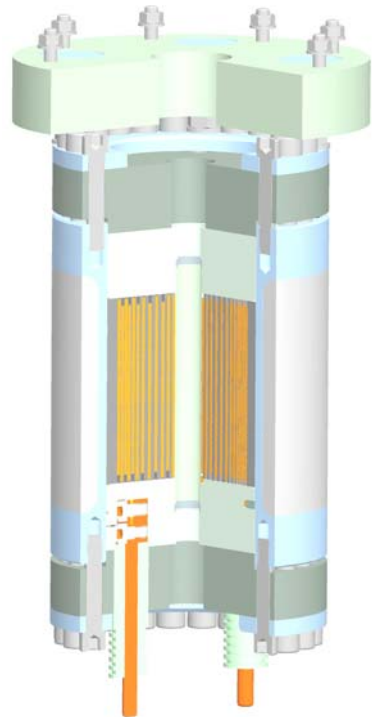
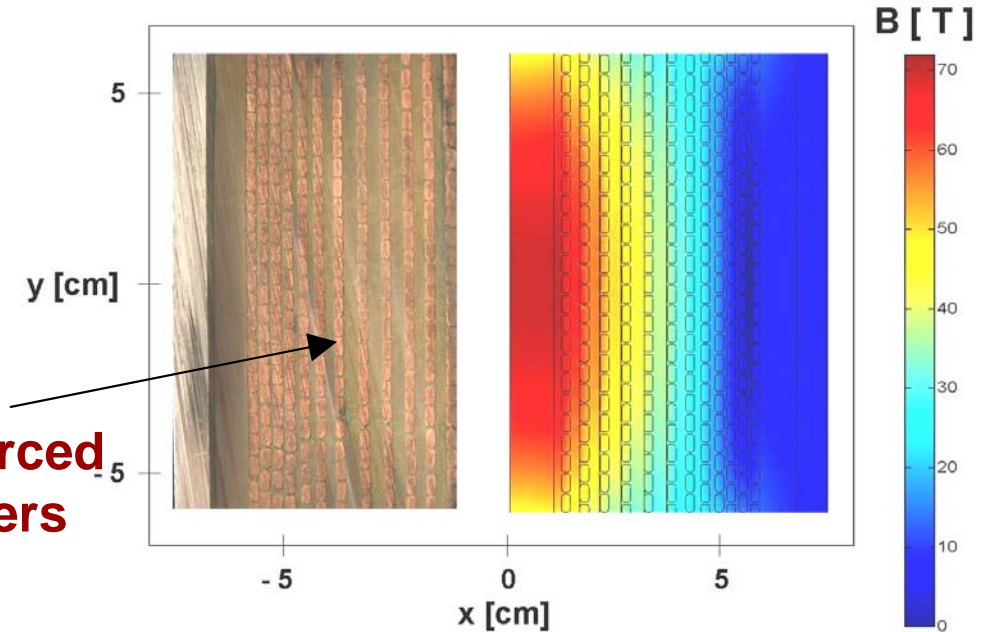


FEA example 1 (azimuthal symmetry):

Challenging conditions in pulsed high-field (70 T) coils

- extremely high Lorentz forces and resulting mechanical load
- extreme heat load
- extreme electrical environment

Wires reinforced by fibers



300 turns, 12 layers, 3 mH,
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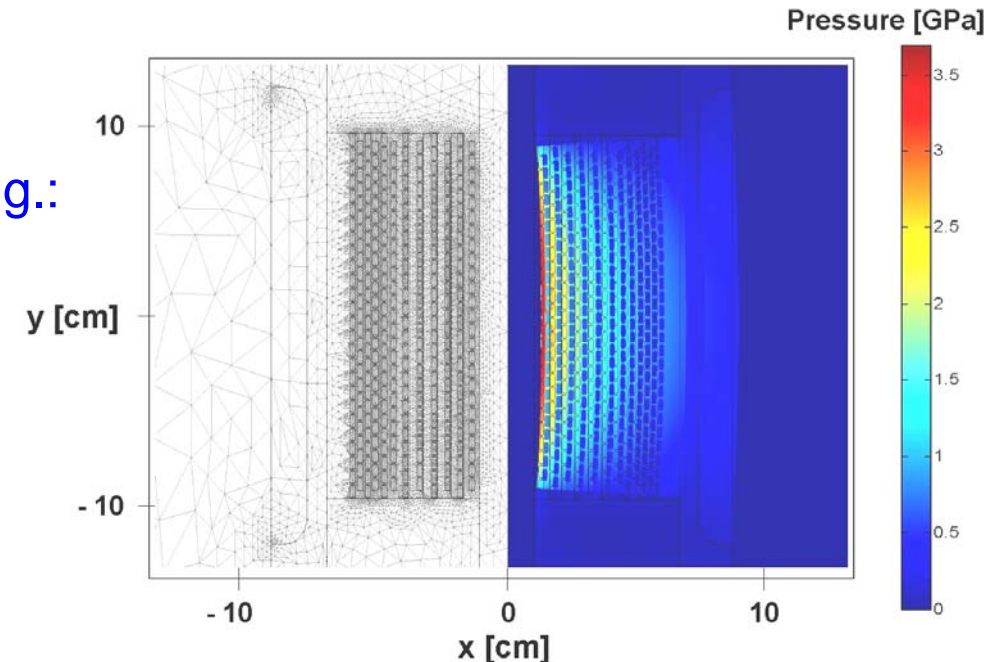
FEA allows for calculation of, e.g.:

$B(x, y, z, t)$ up to 72 T

$T(x, y, z, t)$ up to 350 K

$P(x, y, z, t)$ up to ~ 3.7 GPa

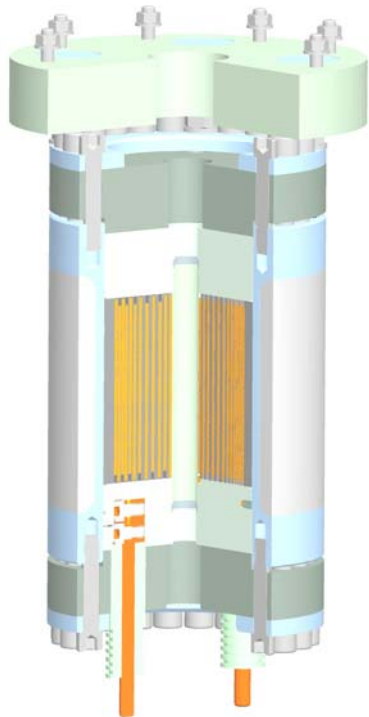
Deformation $dx(t)$, $dy(t)$, $dz(t)$



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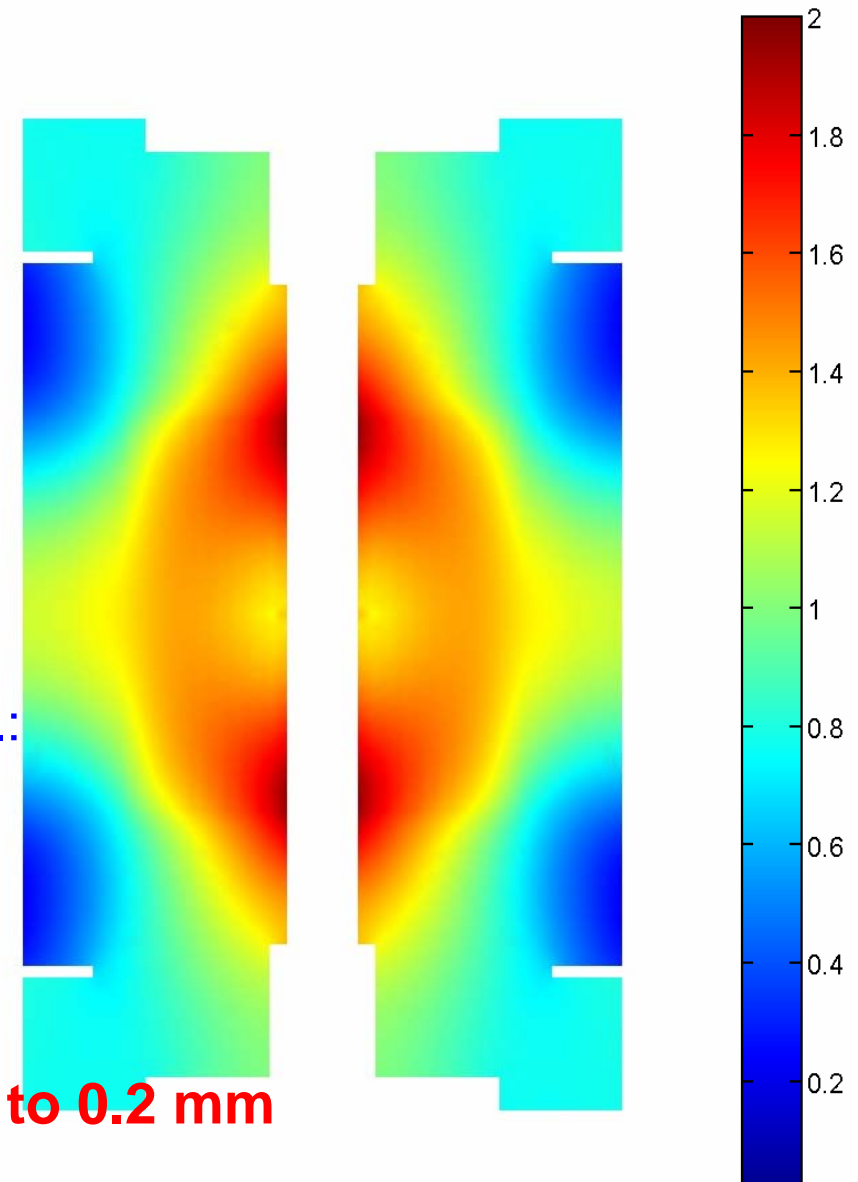
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$T(x, y, z, t)$ up to 350 K

$P(x, y, z, t)$ up to ~ 3.7 GPa

Deformation $dx(t), dy(t), dz(t)$ up to 0.2 mm

Deformation [10^{-4} m]



Challenges

- extremely high Lorentz forces and
- resulting mechanical load
- materials in plastic regime
- extreme heat load
- extreme electrical environment

Special conductors up to ~1 GPa:

- CuSn, CuBe alloys
- CuAl_2O_3 composites
- steel-copper macro composites
- CuAg micro composites
- CuNb nano filament composites

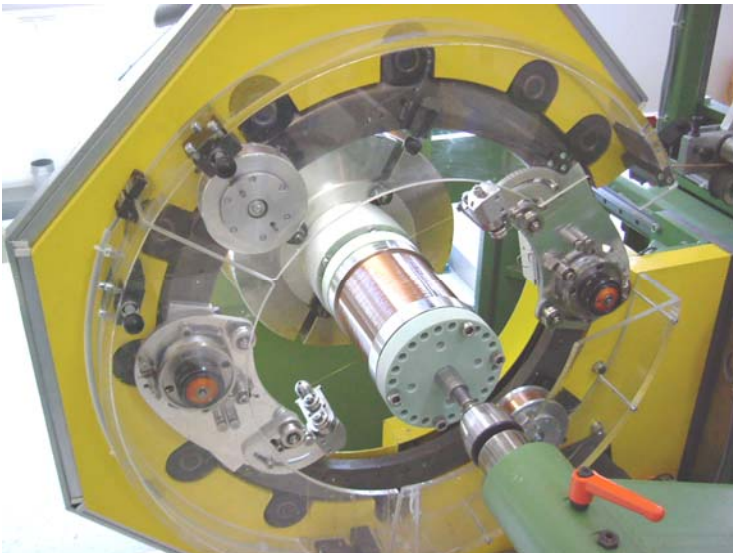
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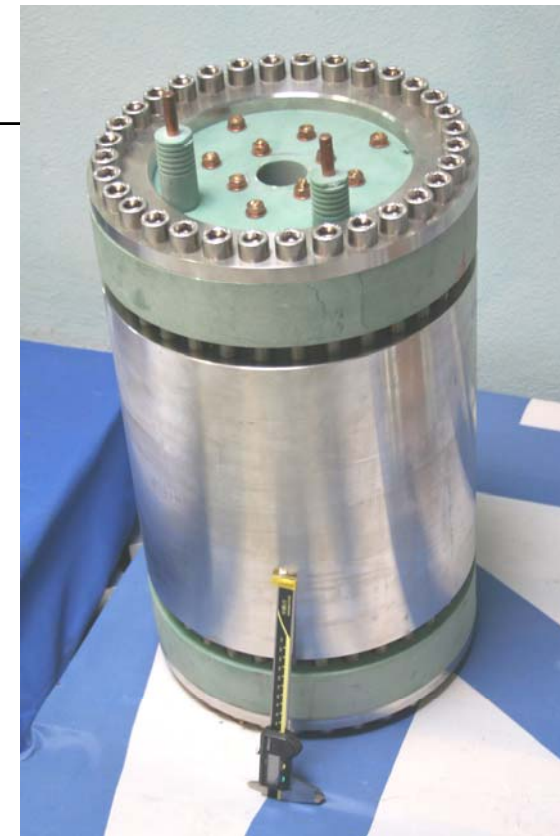
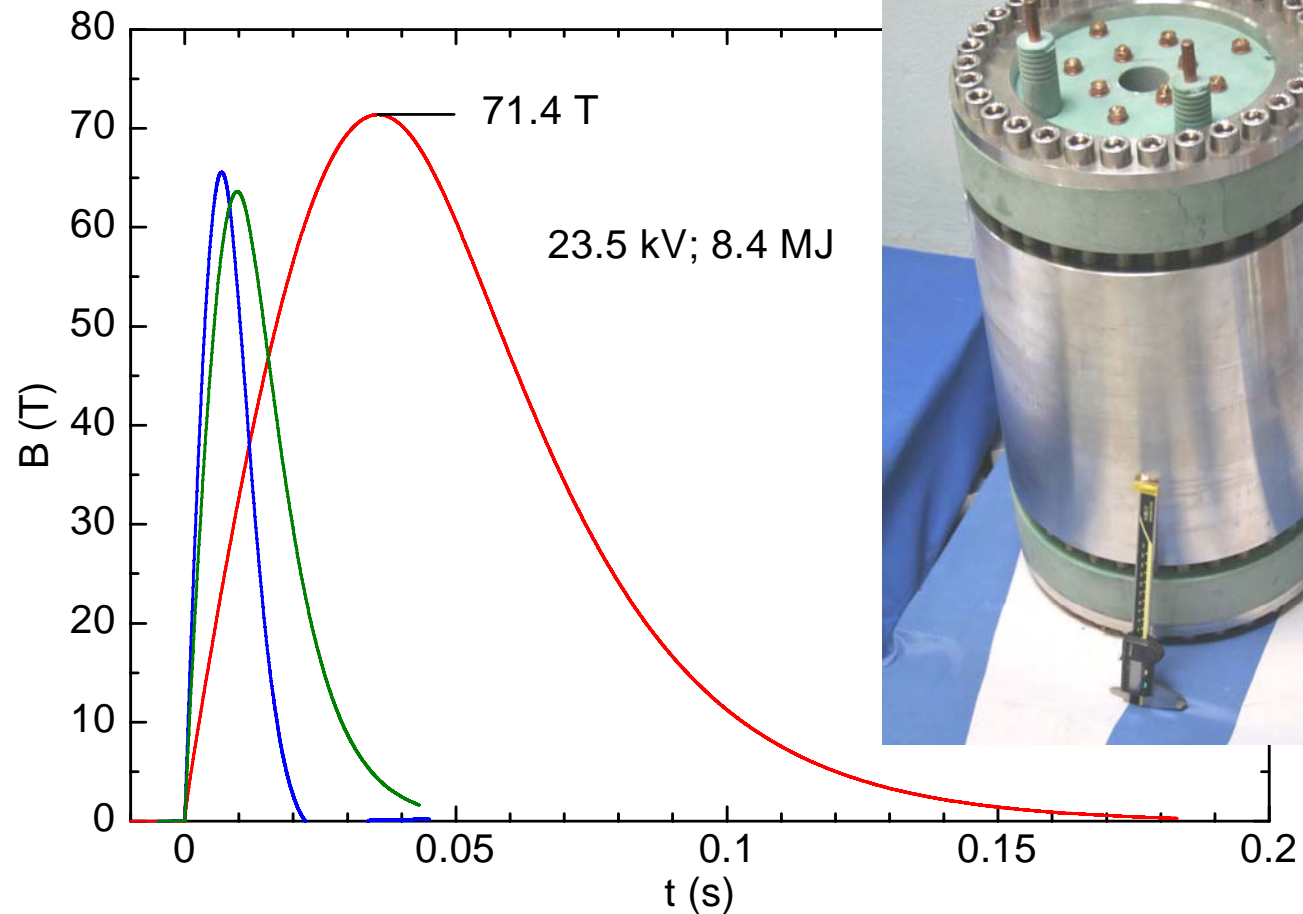
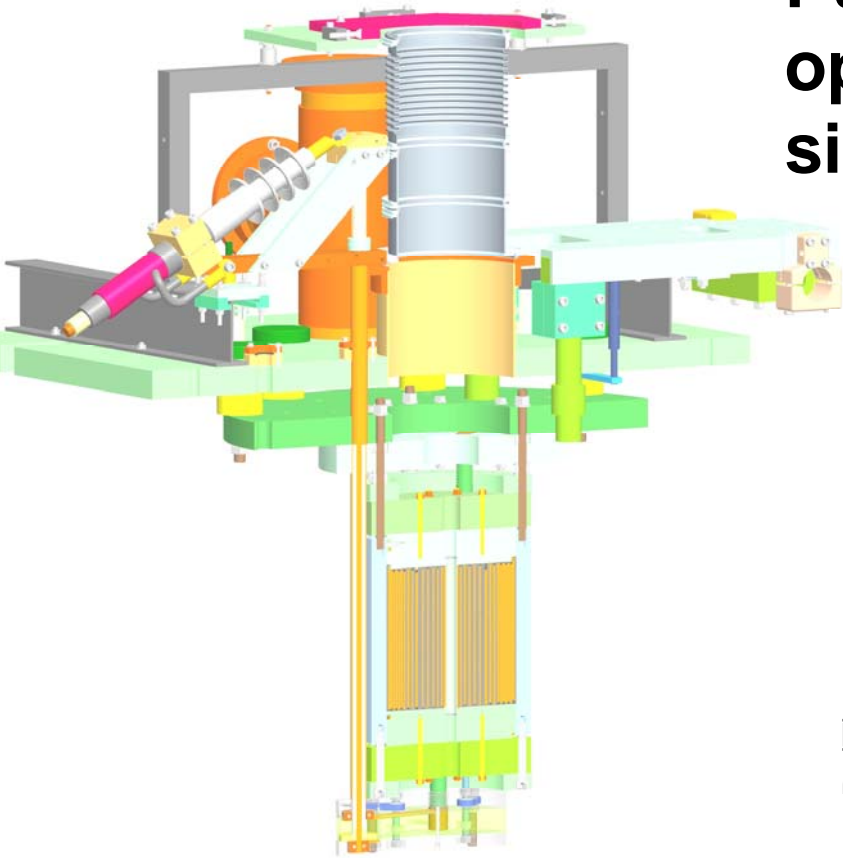
- CuSn, CuBe alloys
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Special fiber reinforcement:

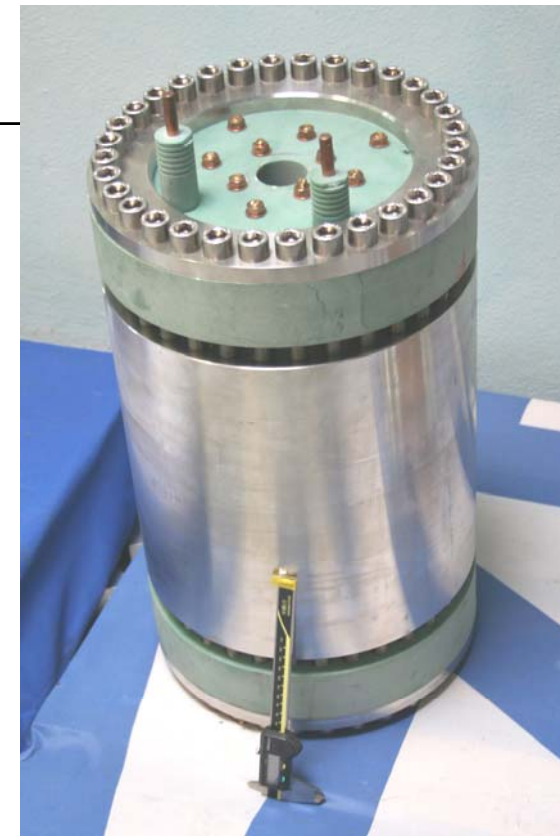
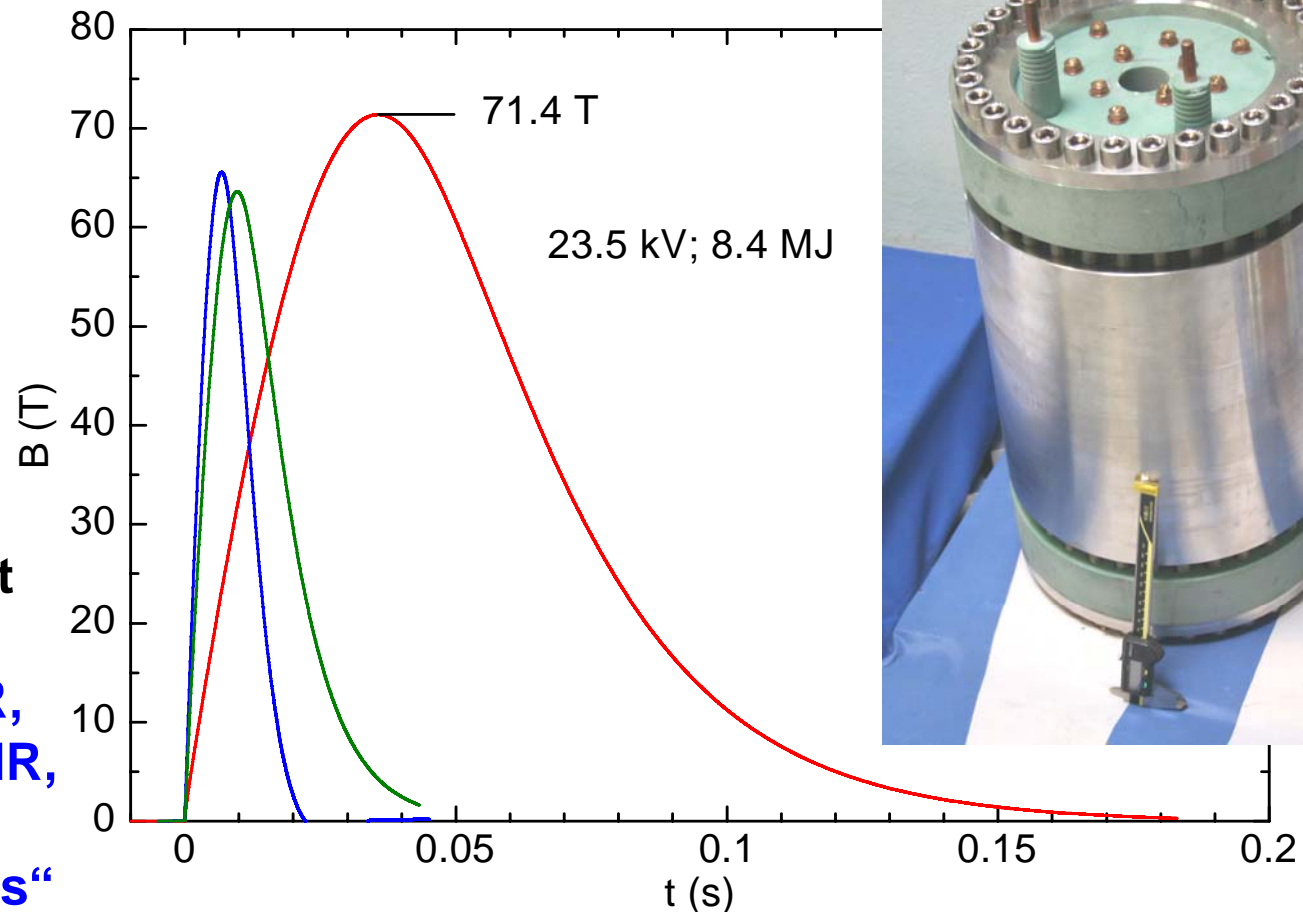
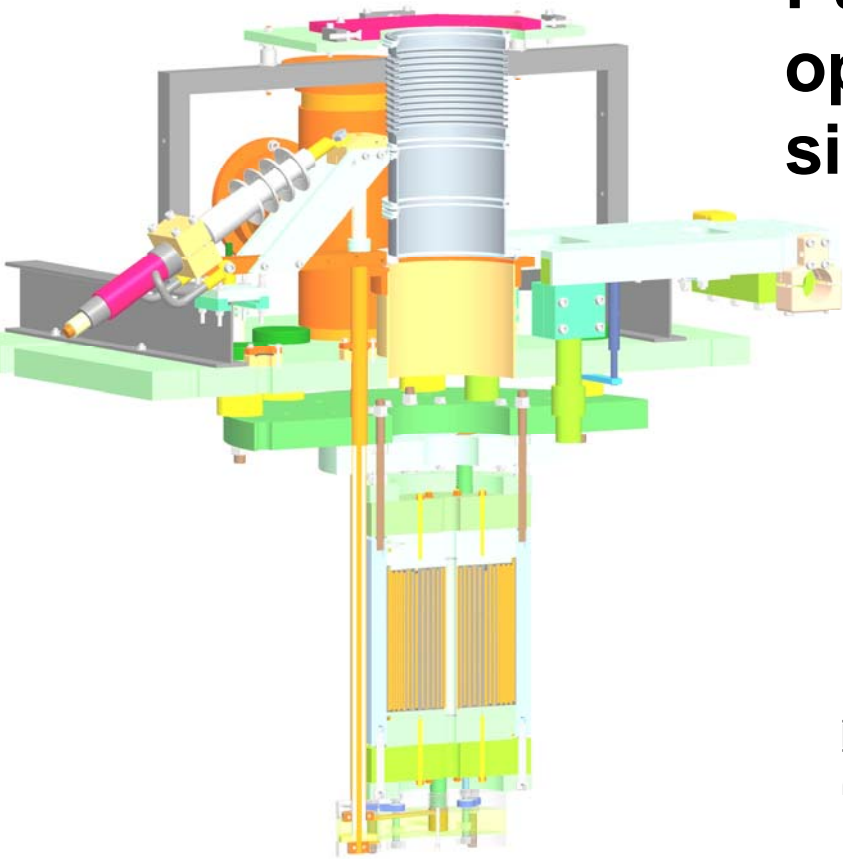
- „Zylon“ (PBO) fiber
- high tensile strength (5 GPa along fibre)
highly anisotropic (consider in FEA !)
- high thermal stability and conductivity
- high-voltage electrical insulation

Steel reinforcement: „MP35N“

Pulsed-field coils of the HLD in continuous operation for internal and external users since 2006:

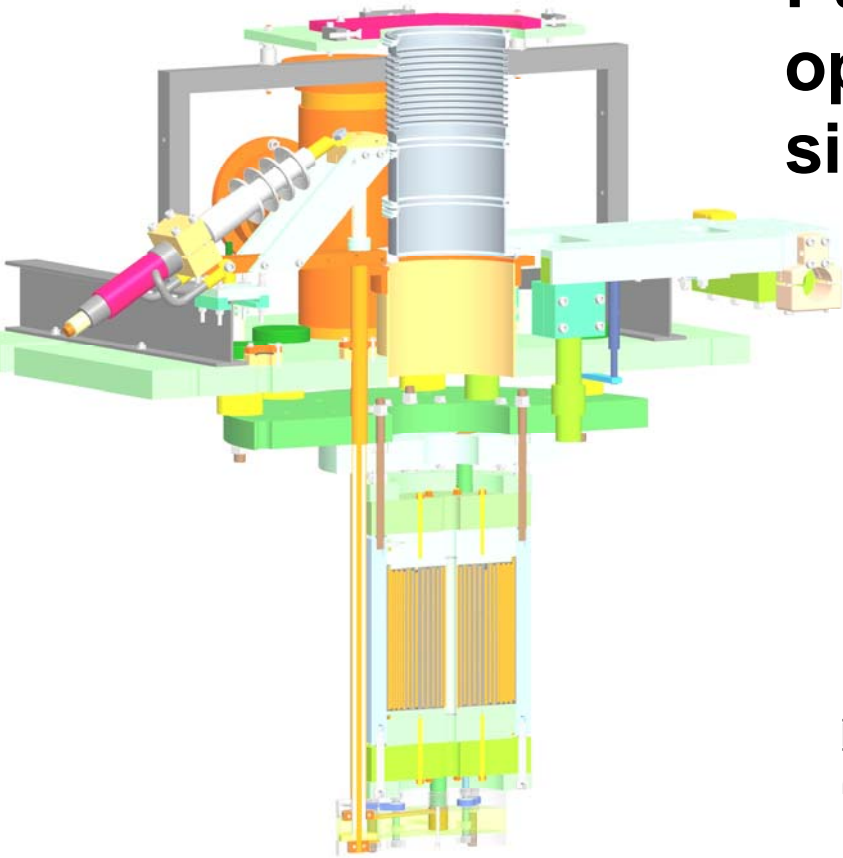


Pulsed-field coils of the HLD in continuous operation for internal and external users since 2006:

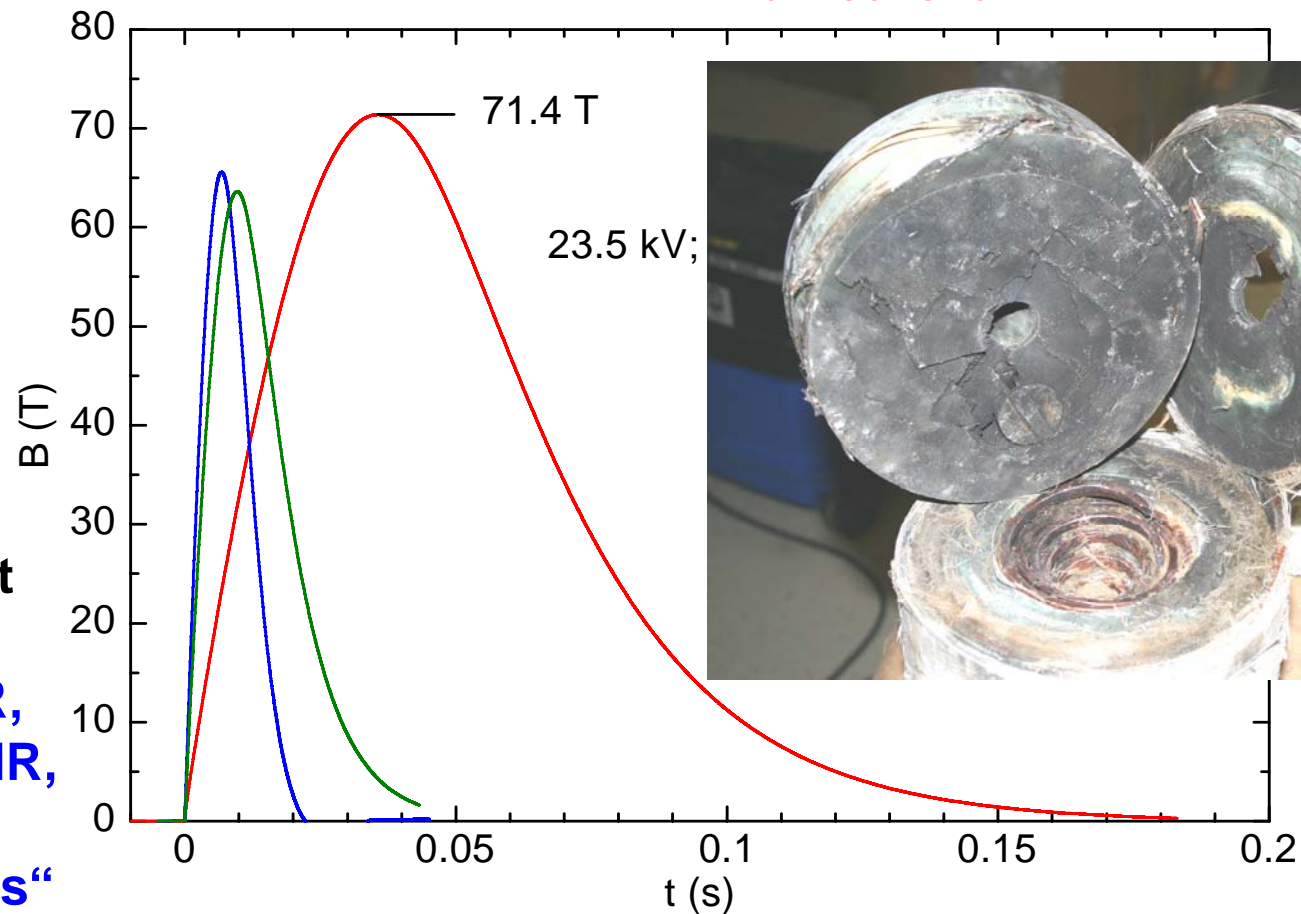


Many experimental measurement techniques available at HLD:
 el. transport, magnetization, ESR, IR spectroscopy, ultrasound, NMR, heat capacity, ...
 „allows for a lot of physics“

Pulsed-field coils of the HLD in continuous operation for internal and external users since 2006:



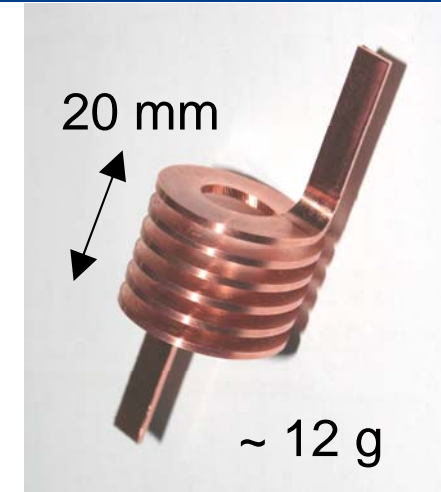
Study of a failure case, ...
„feedback and motivation
for realistic FEA“



Many experimental measurement techniques available at HLD:
el. transport, magnetization, ESR, IR spectroscopy, ultrasound, NMR, heat capacity, ...
„allows for a lot of physics“

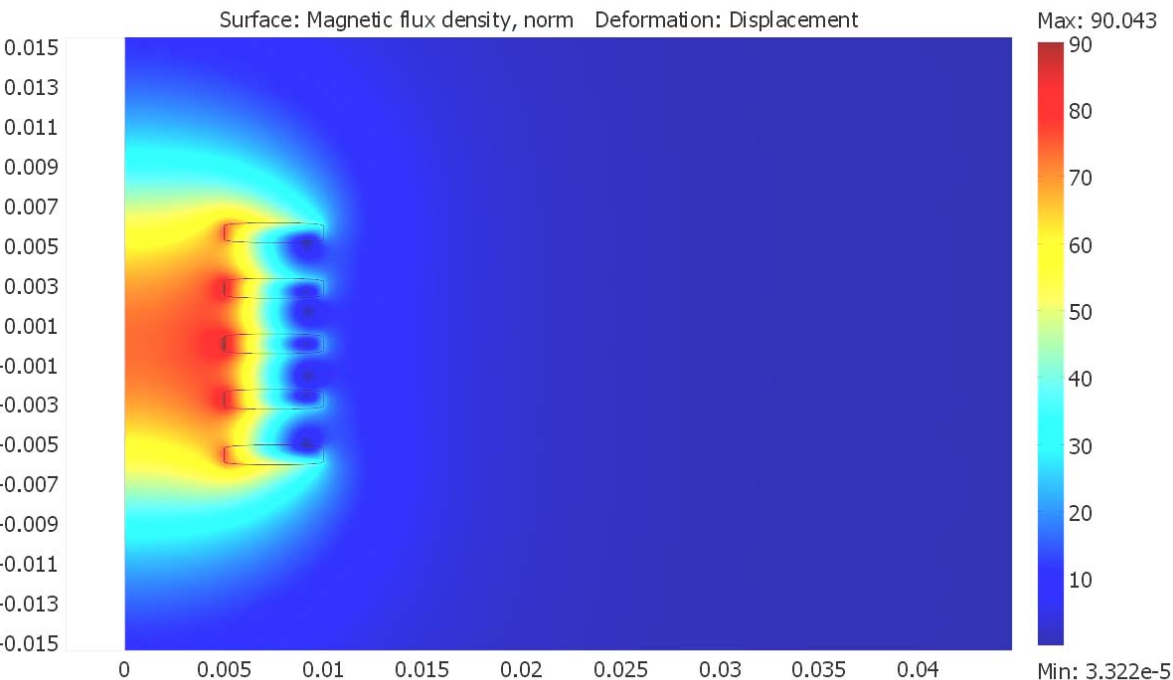
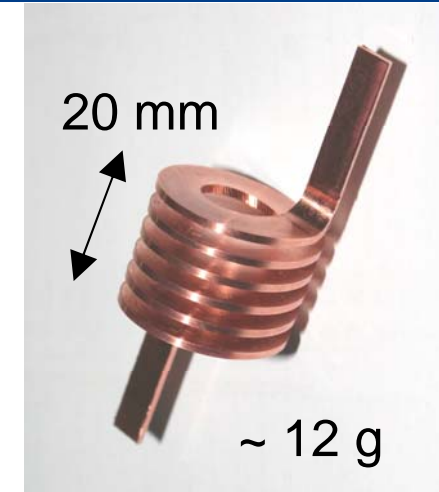
FEA example 2 (2D azimuthal and 3D symmetry):

Five-turn test coil: 5.5 turns, 10 mm bore, $I = 250$ kA, $t_{\text{pulse}} = 10$ μsec



FEA example 2 (2D azimuthal and 3D symmetry):

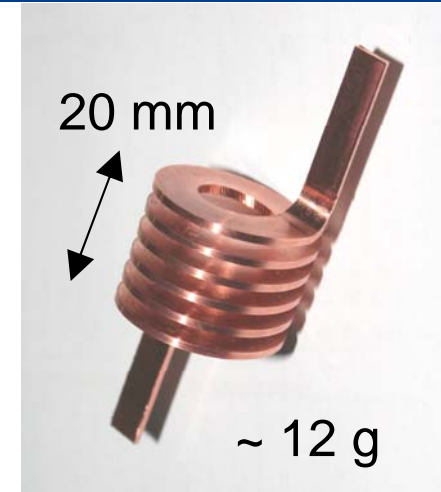
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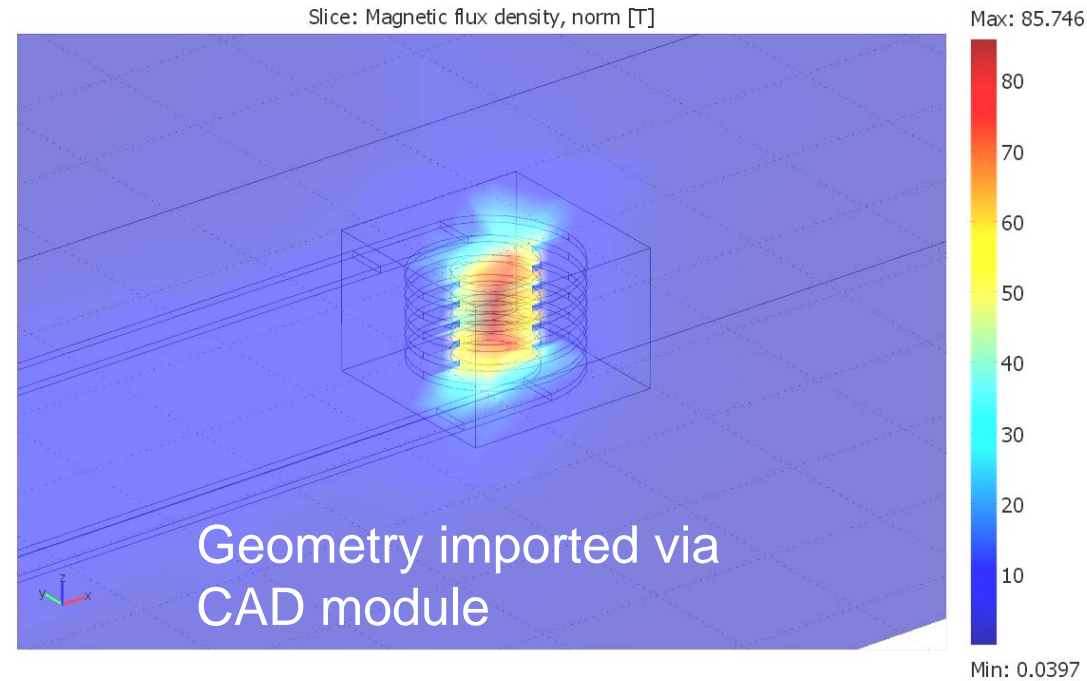
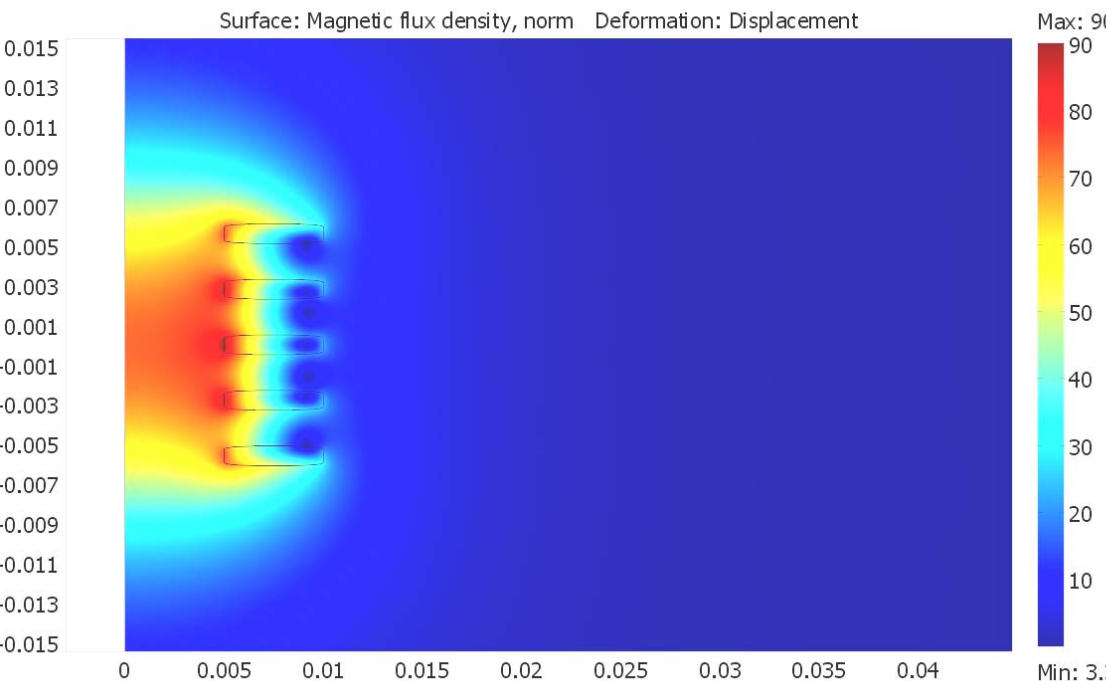
3) Simulation of pulsed-field coils for ultimate flux densities

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Good agreement between 2D and 3D simulation results of $B(r,t)$



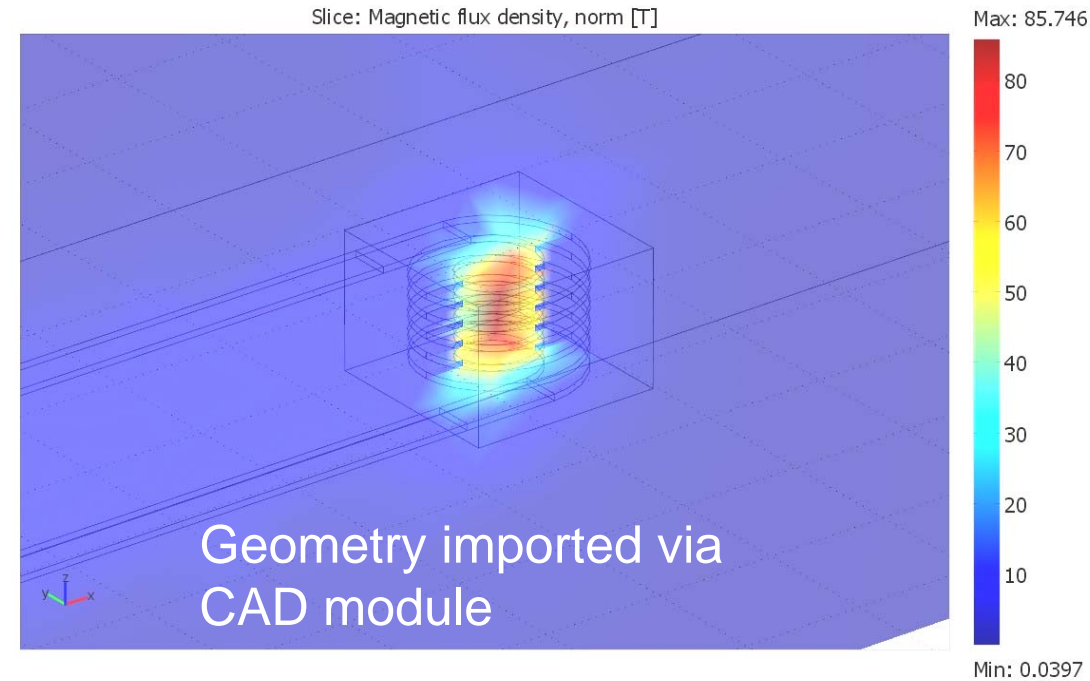
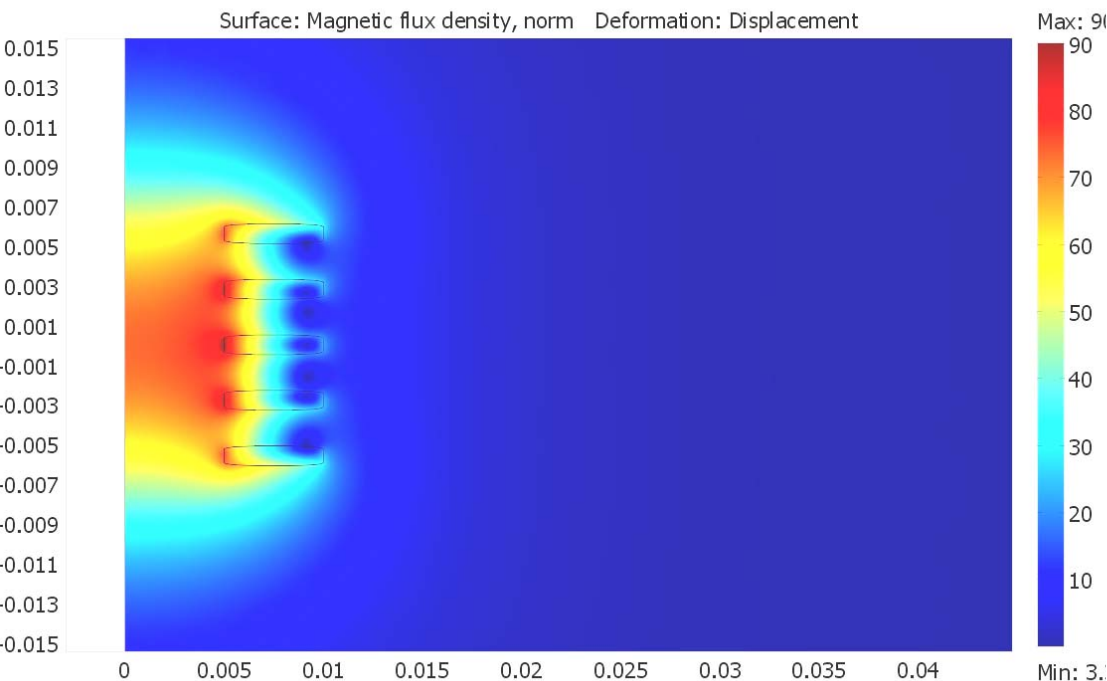
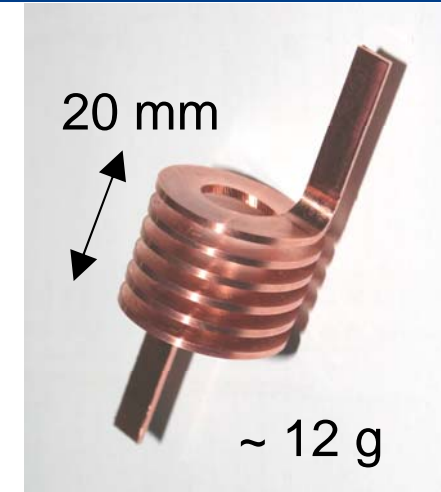
3) Simulation of pulsed-field coils for ultimate flux densities

FEA example 2 (2D azimuthal and 3D symmetry):

Five-turn test coil: 5.5 turns, 10 mm bore, $I = 250$ kA, $t_{\text{pulse}} = 10$ μsec

- Lorentz forces and mechanical load cause plastic deformation at fields > 50 T
- heat up to $T_{\text{max}} > 400$ K critical for fiber composite
- critical electrical-field gradients between windings (kV/mm)

Good agreement between 2D and 3D simulation results of $B(r,t)$

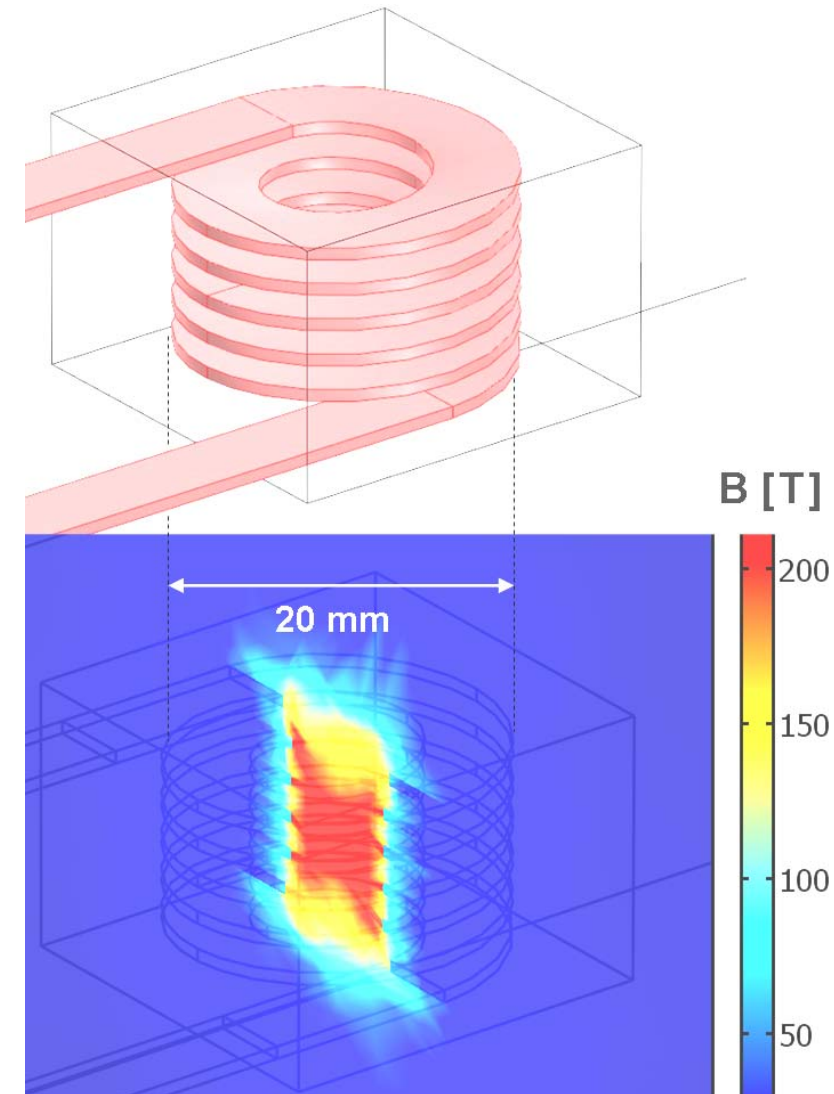


FEA example 2 (2D azimuthal and 3D symmetry):

Five-turn test coil: 5.5 turns, 10 mm bore, **$I = 600 \text{ kA}$** , $t_{\text{pulse}} = 10 \mu\text{sec}$

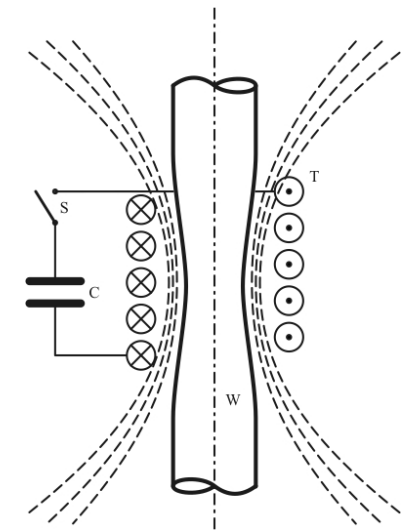
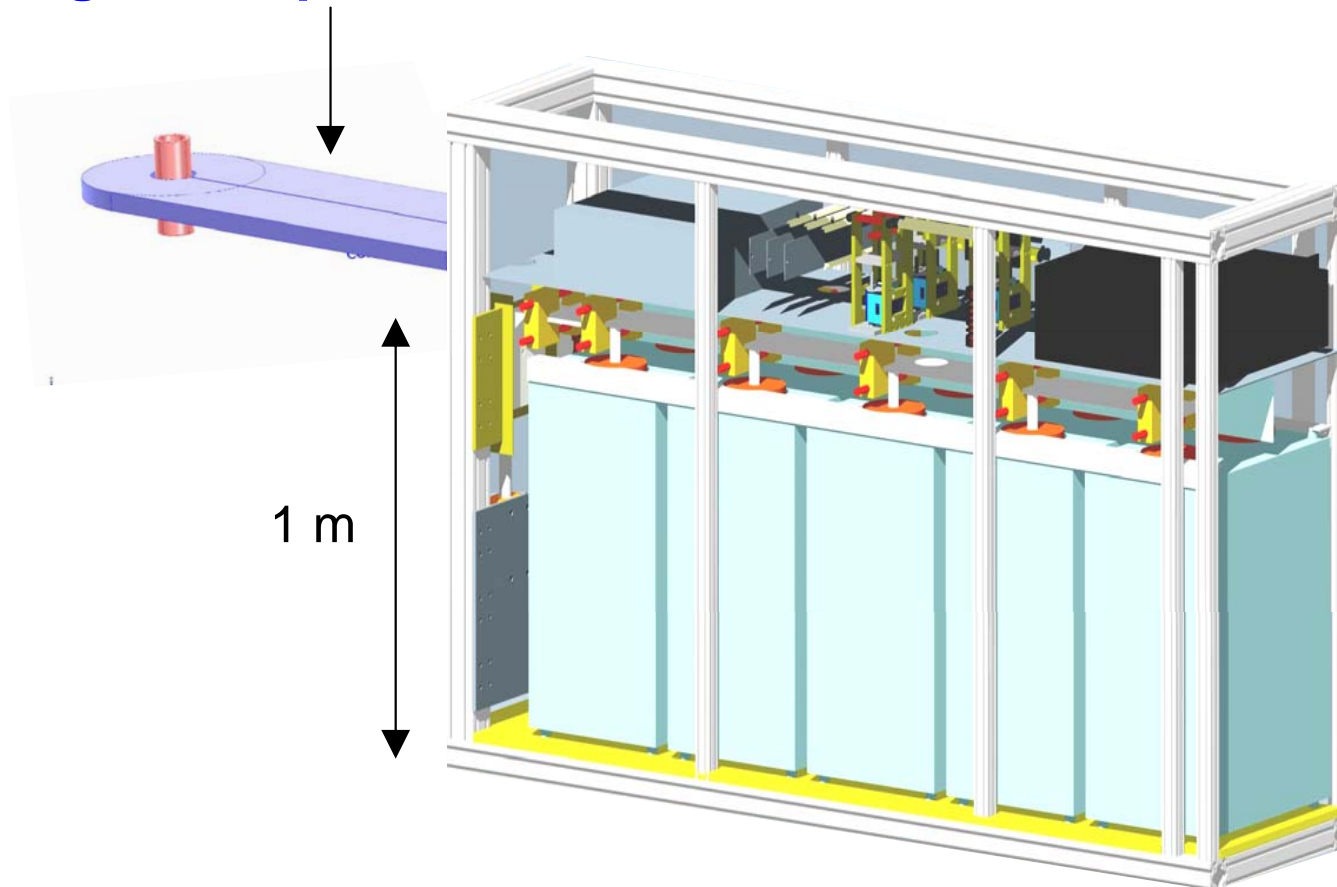
- magnetic flux densities $> 100 \text{ T}$ feasible in the μsec time range
 $B = 220 \text{ T}$
- Lorentz forces beyond destructive limits,
 $P > 5 \text{ GPa}$
- possible melting and evaporation of coil
- critical electrical-field gradients between windings (kV/mm)

Multiphysics FEA needed for modelling and optimization of the field pulse and burst of the coil



FEA example 3 (3D simulation):

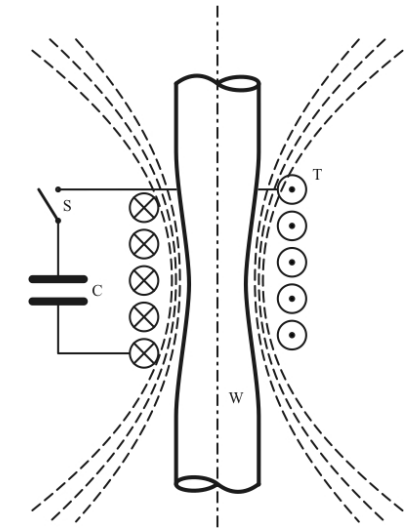
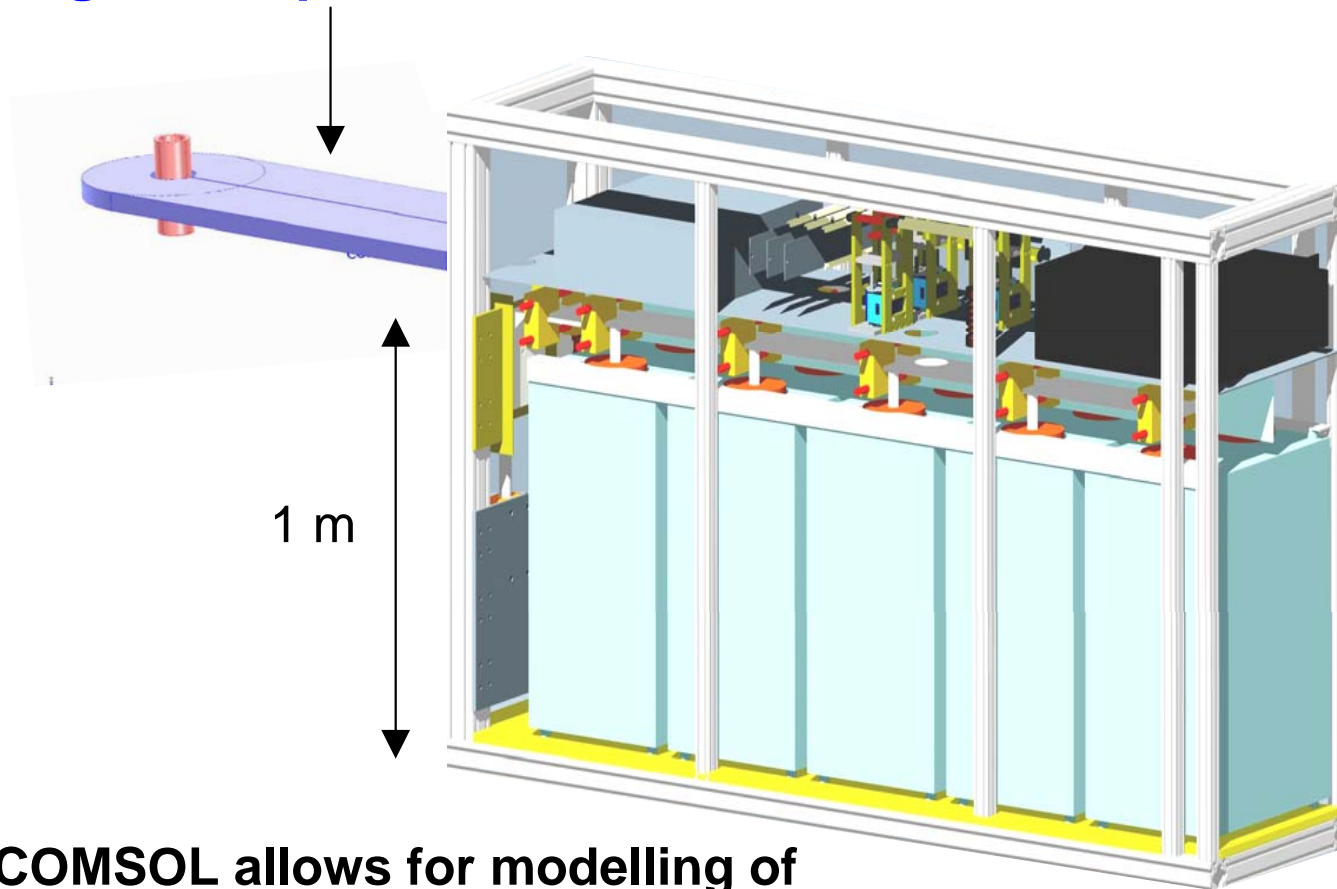
Single-turn pulse deformation coil:



**Pulse-current generator
(discharge capacitor bank)**

FEA example 3 (3D simulation):

Single-turn pulse deformation coil:



**Pulse-current generator
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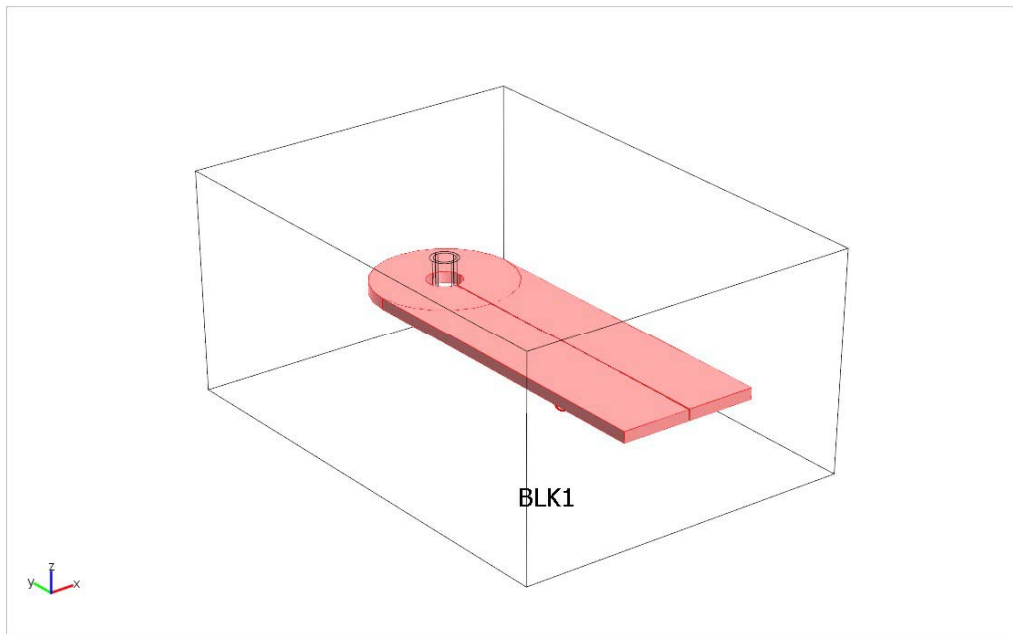
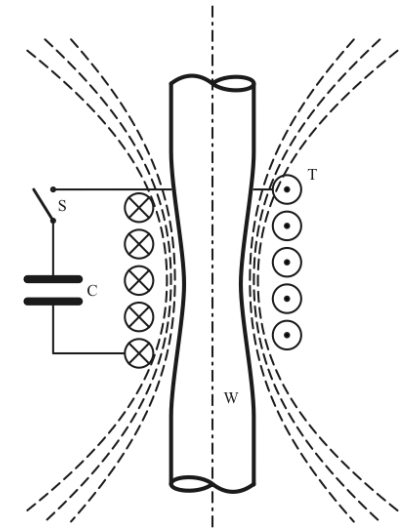
COMSOL allows for modelling of

- electromagnetic pulse forming process, i. e. Lorentz forces on induced eddy currents
- basic properties of the pulse generator: inductance ~ 100 nH of the high-power circuit

FEA example 3 (3D simulation):

Single-turn pulse deformation coil:

single turn, 52 mm (2 inch) bore, 2mm slit, 20 mm x 100 mm bars, 600 mm length, $I = 500 \text{ kA}$, $t_{\text{pulse}} = 10 \mu\text{sec}$

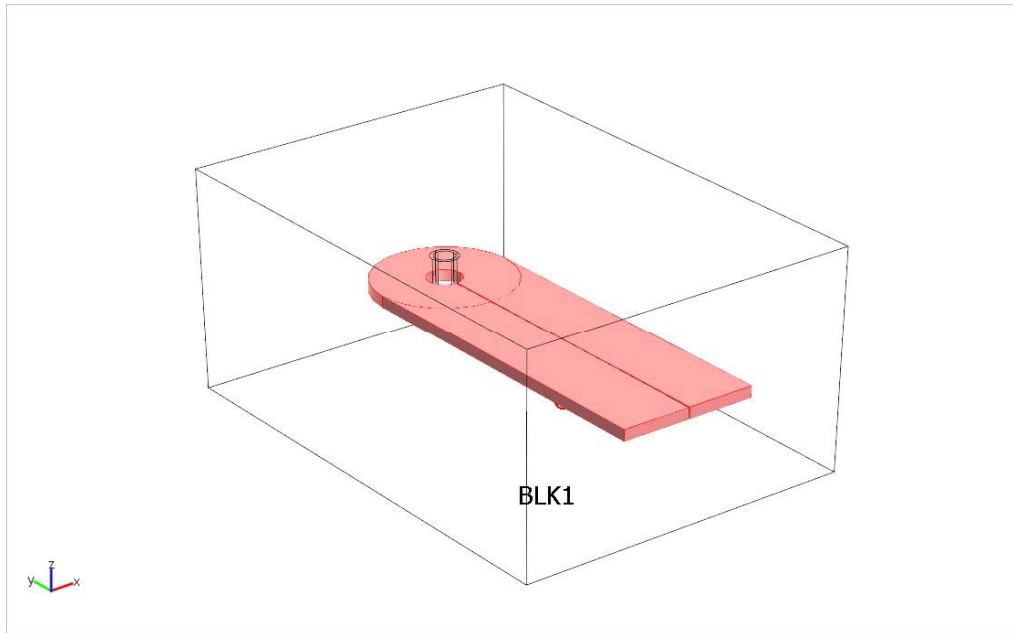
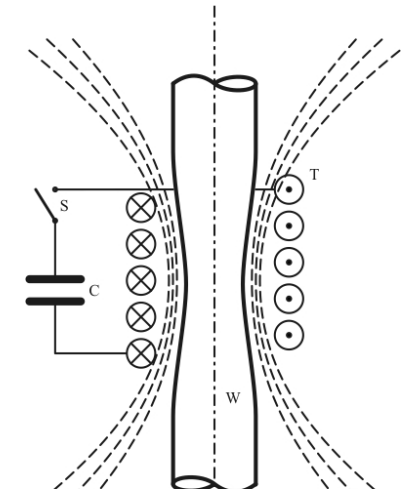


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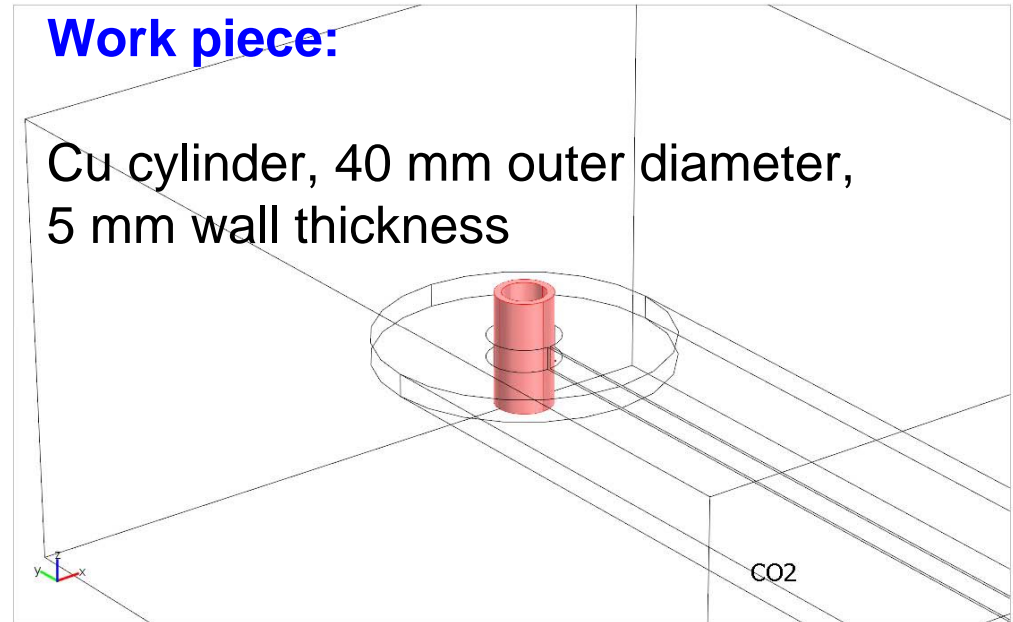
single turn, 52 mm (2 inch) bore, 2mm slit, 20 mm x 100 mm bars, 600 mm length, $I = 500 \text{ kA}$, $t_{\text{pulse}} = 10 \mu\text{sec}$

- Lorentz forces on induced eddy currents cause plastic deformation of work piece
- challenging electrical environment

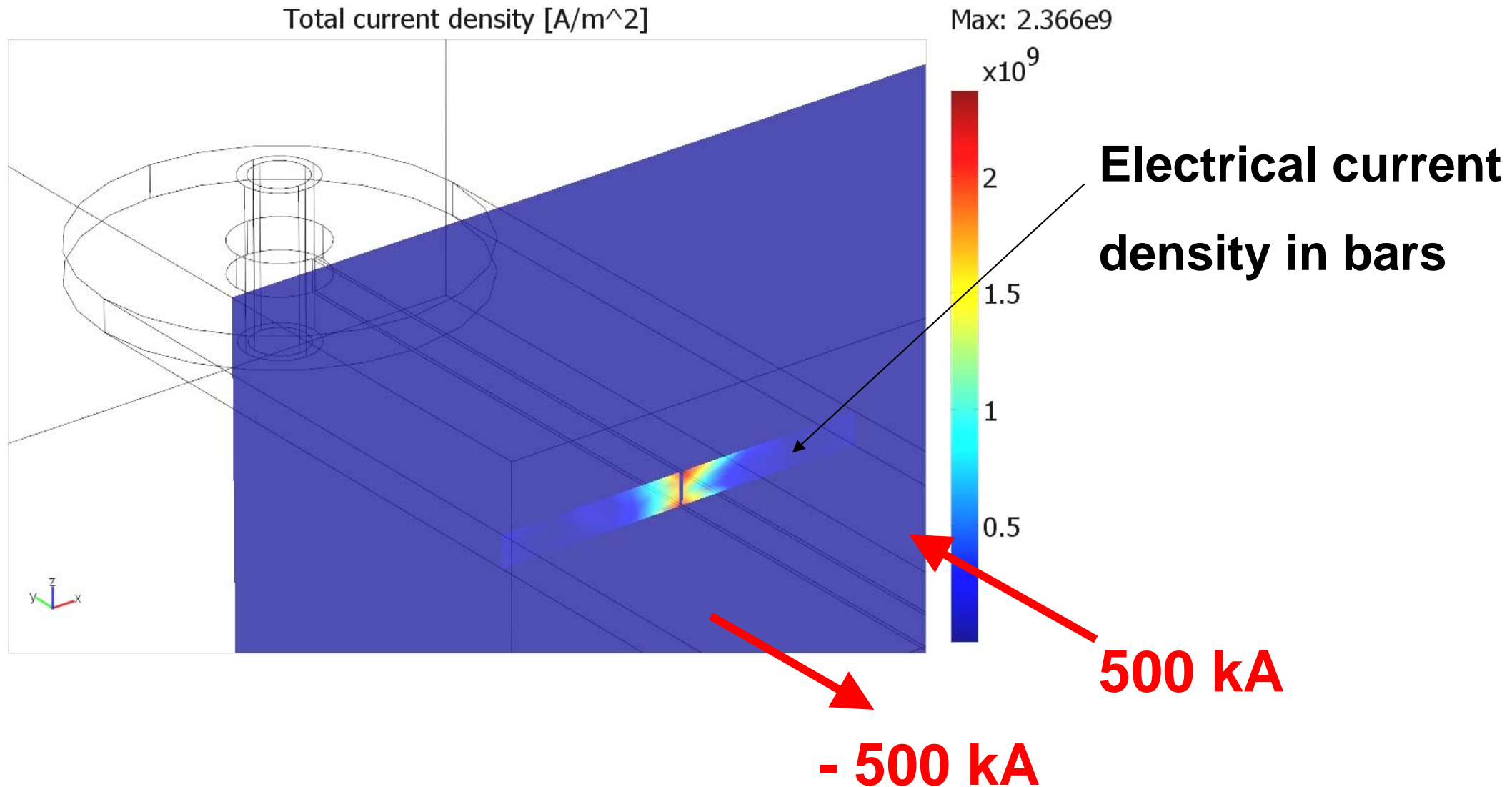


Work piece:

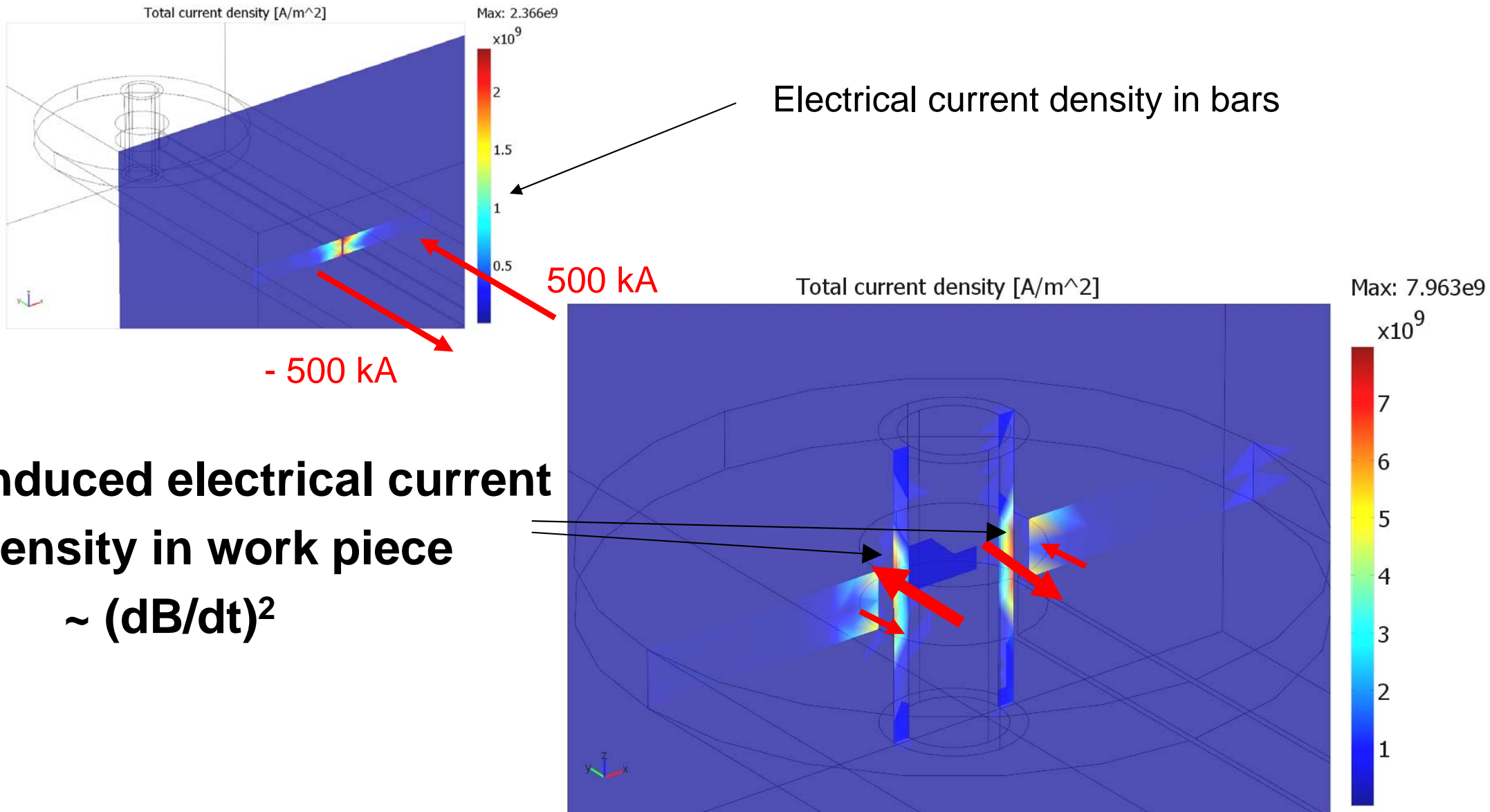
Cu cylinder, 40 mm outer diameter, 5 mm wall thickness



FEA example 3 (3D simulation): Single-turn pulse deformation coil:



FEA example 3 (3D simulation): Single-turn pulse deformation coil:

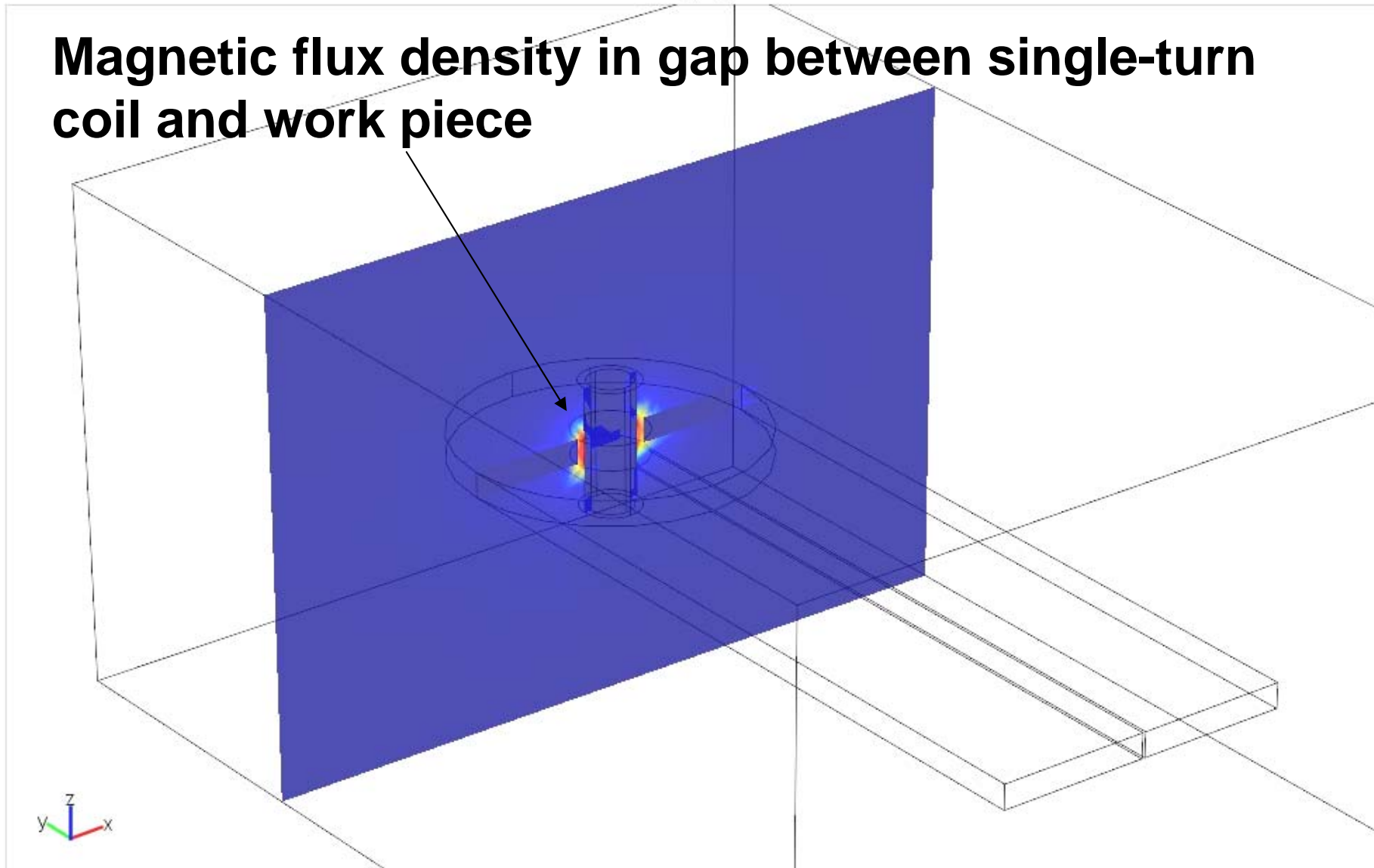


Induced electrical current density in work piece
 $\sim (dB/dt)^2$

FEA example 3 (3D simulation): Single-turn pulse deformation coil:

B [T]

Magnetic flux density in gap between single-turn coil and work piece



Max: 16.0

16

14

12

10

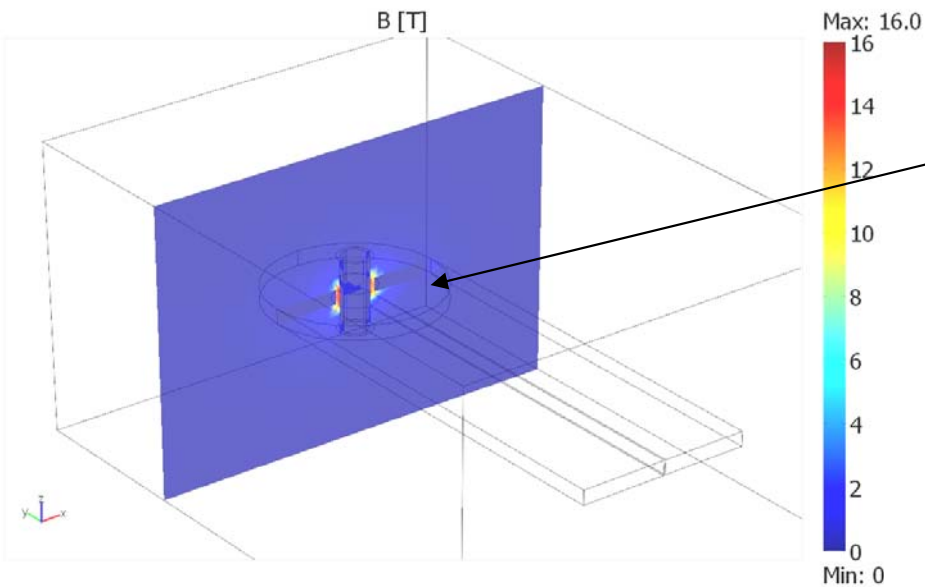
8

6

4

2

FEA example 3 (3D simulation): **Single-turn pulse deformation coil:**



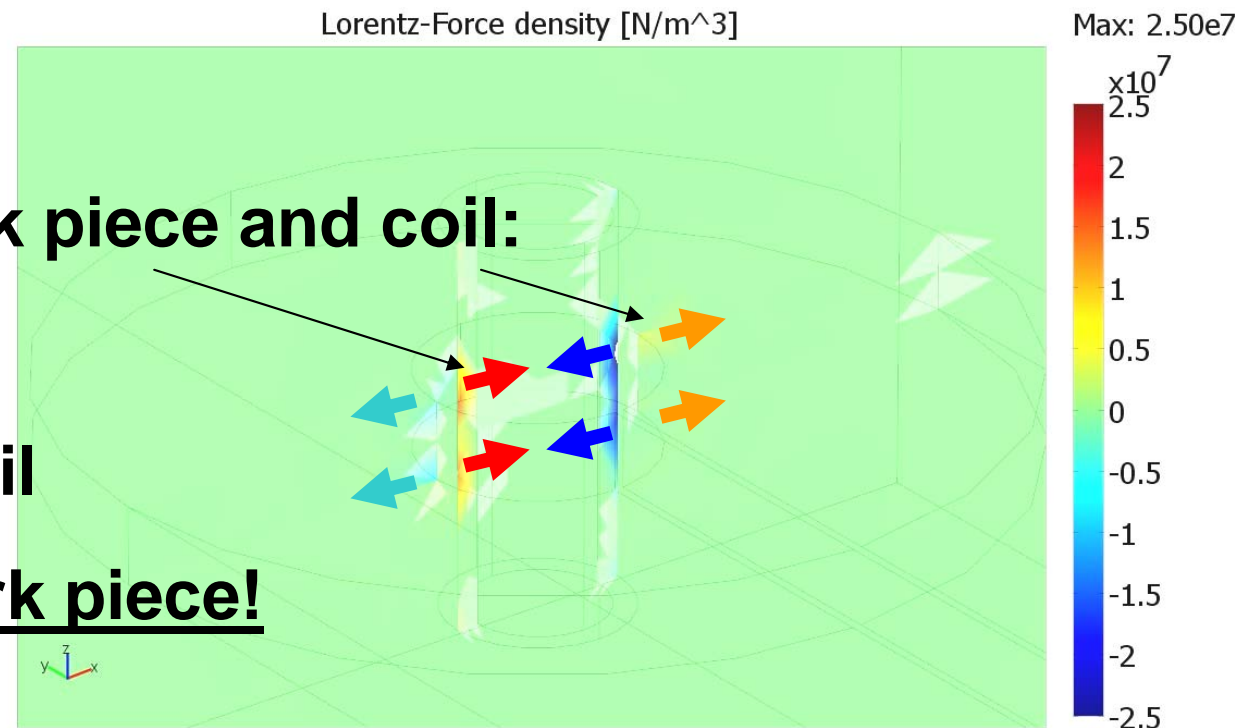
Magnetic flux density in gap between single-turn coil and work piece

Lorentz force density in work piece and coil:

$$\underline{F} / V = \underline{J} \times \underline{B}$$

-> radial expansion of the coil

-> radial compression of work piece!



FEA example 3 (3D simulation): Single-turn pulse deformation coil:

Lorentz force density in work piece and coil:

$$\underline{F} / V = \underline{J} \times \underline{B}$$

-> radial expansion of the coil

challenges:

- high repetition rate (≤ 10 sec)
- long life time ($\geq 10^6$ pulses)
- coil needs elastic regime

-> radial compression of work piece!

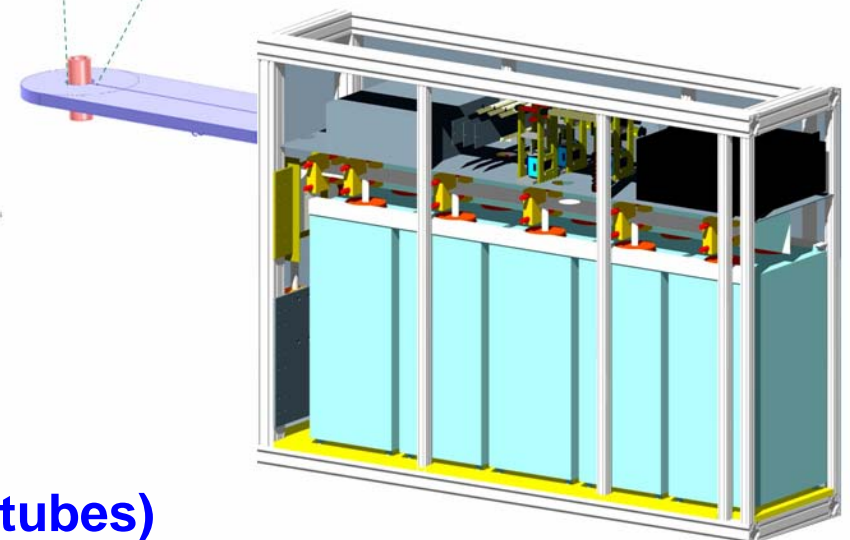
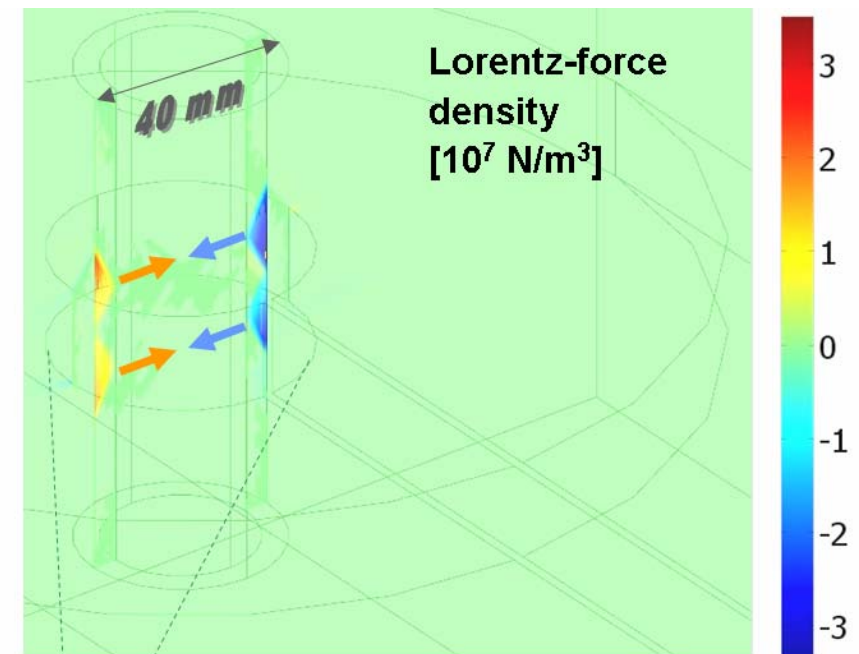
Next steps:

FEA of mechanical load:

- workpiece needs plastic regime
- use of real stress-strain curve
- calculation of plastic deformation

No limits for geometry !

Future: FEA of welding processes (e. g. of coaxial tubes)



Finite Element Analysis (FEA) has emerged to an important tool

- to evaluate pulsed- power and pulsed-magnetic field techniques which are a technology platform for modern research and novel industrial innovations.

-Thanks to its stepwise improvement during the recent years, COMSOL offers many features to simulate the physical behavior of even larger structures, such as pulsed magnetic field coils made of various parts of materials or composites with very different quantities (iso- or anisotropic functions of temperature, field, pressure, ...)

- For this purpose, the possibility to perform simulations which comprise several differential equations from many disciplines of physics (multi-physics), such as electrodynamics, mechanics, and thermo-dynamics is beneficial.

- COMSOL also allows for a computation of quantities which are associated with the design of electrical circuits, such as the inductance of components without any restriction of their shape. For this reason, COMSOL can be also used to describe pulsed power generators and the technique of electromagnetic pulse forming, joining and possibly welding.

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EU projects:

- EuroMagNET
- DeNUF
- MAGISTER
- EuroMagNET-II
- Upgrade
ESFRI roadmap



International conference
 “Research at High Magnetic Fields”
 HLD, Dresden, July 2009



Institute for Complex
 Adaptive Matter