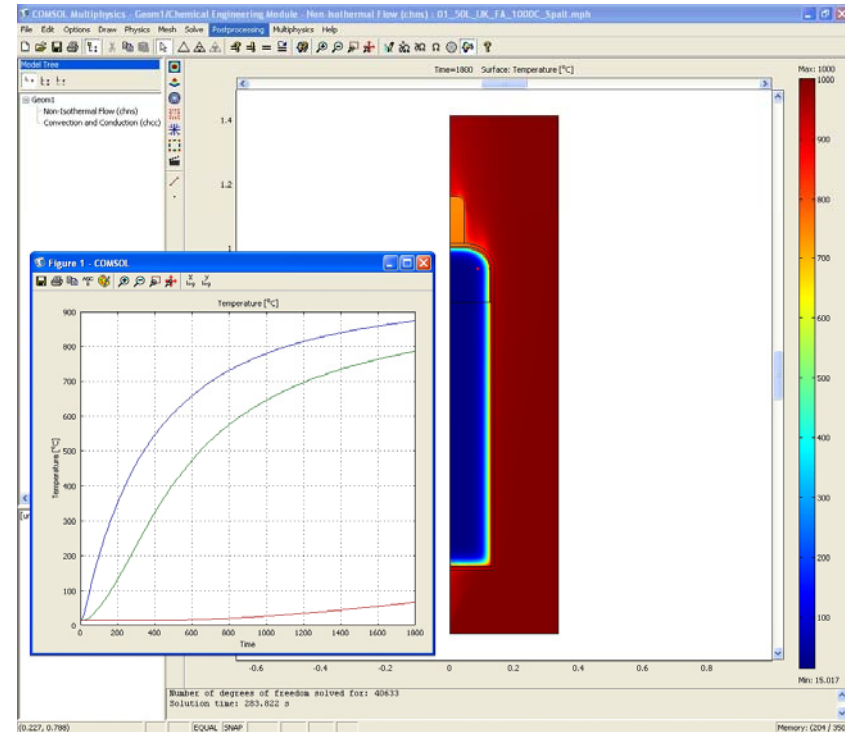


COMSOL Multiphysics as a Tool to Increase Safety in the Handling of Acetylene Cylinders Involved in Fires

Fabio Ferrero

BAM Federal Institute for Materials Research and Testing
Division II.1 "Gases, Gas Plants"
Working Group "Safety Related Properties of Gases"
Unter den Eichen 87, D-12205 Berlin, Germany

COMSOL CONFERENCE
Milan, October 14-16 2009



Background

- Acetylene (C_2H_2) is commonly used for cutting and welding purposes
- Normally stored in compressed gas cylinders
- Acetylene cylinders involved in fire can burst



Explosion of a fully charged 40 dm³ acetylene cylinder (bonfire test)

- Previous accidents:
 - Schutterwald, Germany, accident in a private workshop (1994)
 - Brisbane, Australia, accident in an acetylene factory (1999)
 - Dallas, USA, accident in a gas factory (2007)

Consequences

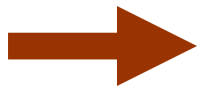


Economical and human losses (fireball, ejection of fragments)

Objectives

Important to know:

- *heating up process*
 - time to explosion
- *critical temperature / pressure in the cylinder*
 - acetylene can decompose with high heat release (226 kJ/mol)
- *cooling with water*
 - the cylinder can be safely handled after the fire



experiments and/or simulations

A mathematical model to predict the heat transfer in the acetylene cylinder has been developed and solved in COMSOL Multiphysics

Acetylene Cylinder

Acetylene cylinder:

- steel wall
- the inside is not a free space, but a complex system



Acetylene Cylinder

Composition cylinder inside:

- porous material
- acetone (liquid/vapour)
- acetylene (free/dissolved)



Acetylene Cylinder

Composition cylinder inside:

- porous material
- acetone (liquid/vapour)
- acetylene (free/dissolved)

Free space

- free acetylene
- acetone vapour



Simulation: geometry & mesh

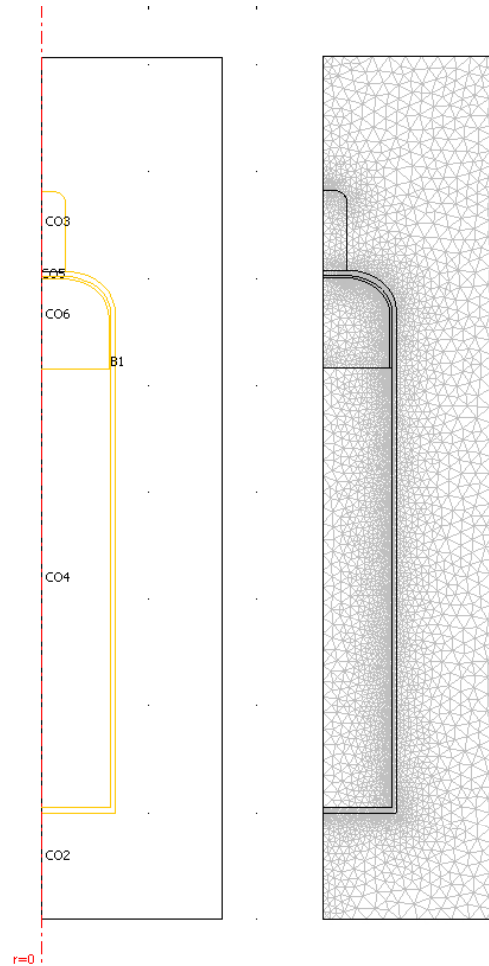
Implementation in COMSOL

Geometry (50 dm³):

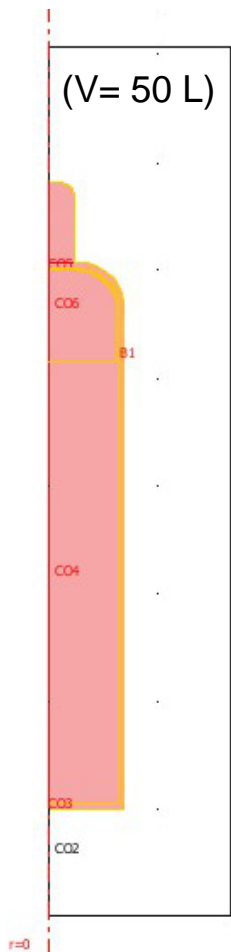
2D Axial symmetric (computing time reduction)

Mesh

- elements: 10740
- nodes: 6045
- degrees of freedom: 40633



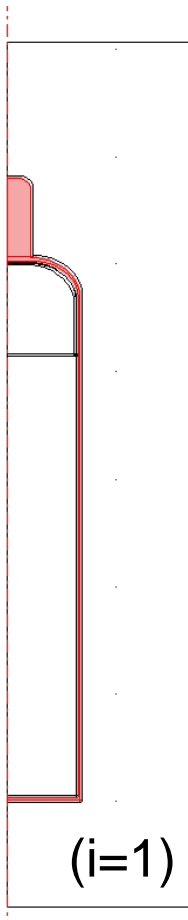
Simulation: domains and equations



Heat transfer through **conduction**

$$\rho_i c_{p,i} \frac{\partial T}{\partial t} = \lambda_i \operatorname{div} \operatorname{grad} T \quad (1)$$

Simulation: domains and equations

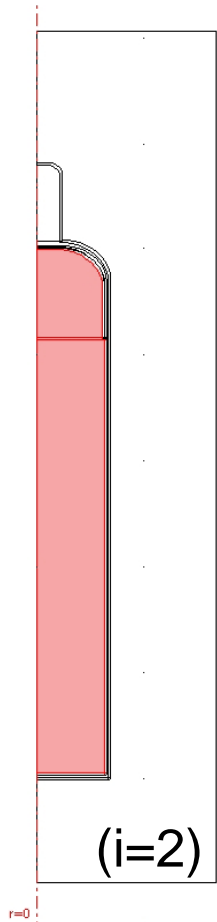


Heat transfer through **conduction**

$$\rho_i c_{p,i} \frac{\partial T}{\partial t} = \lambda_i \operatorname{div} \operatorname{grad} T \quad (1)$$

i=1 steel wall (COMSOL library)

Simulation: domains and equations



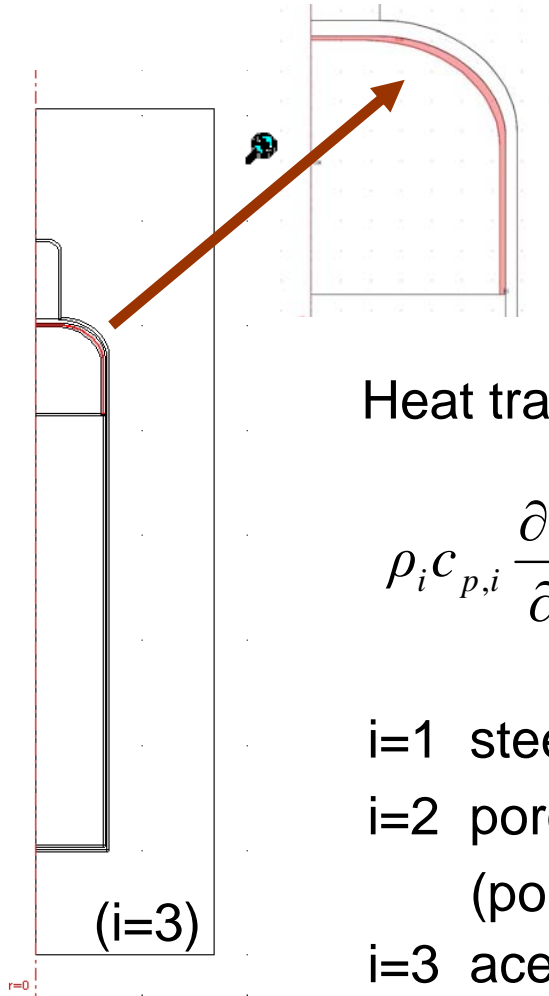
Heat transfer through **conduction**

$$\rho_i c_{p,i} \frac{\partial T}{\partial t} = \lambda_i \operatorname{div} \operatorname{grad} T \quad (1)$$

i=1 steel wall (COMSOL library)

i=2 porous material / acetone (g,l) / acetylene (d,f)
(polynomial functions)

Simulation: domains and equations



Heat transfer through **conduction**

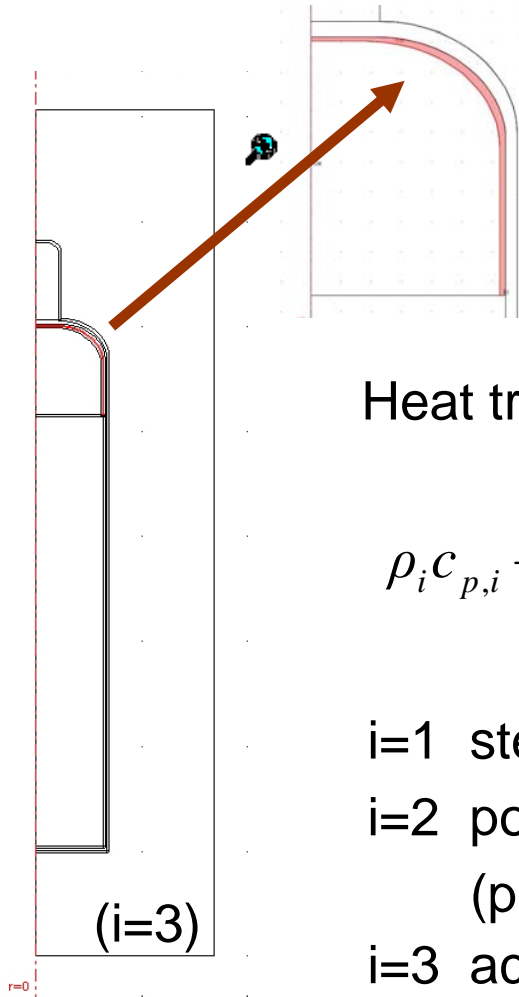
$$\rho_i c_{p,i} \frac{\partial T}{\partial t} = \lambda_i \operatorname{div} \operatorname{grad} T \quad (1)$$

i=1 steel wall (COMSOL library)

i=2 porous material / acetone (g,l) / acetylene (d,f)
(polynomial functions)

i=3 acetylene (g) (polynomial functions)

Simulation: domains and equations



No decomposition / No pressure

Heat transfer through **conduction**

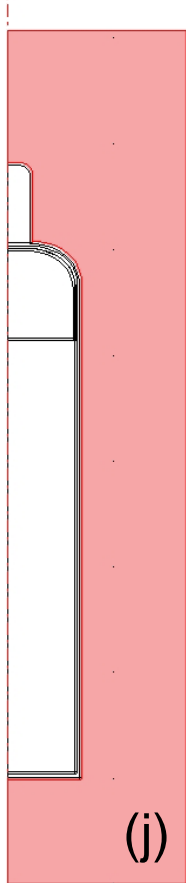
$$\rho_i c_{p,i} \frac{\partial T}{\partial t} = \lambda_i \operatorname{div} \operatorname{grad} T \quad (1)$$

i=1 steel wall (COMSOL library)

i=2 porous material / acetone (g,l) / acetylene (d,f)
(polynomial functions)

i=3 acetylene (g) (polynomial functions)

Simulation: domains and equations



Heat transfer through **conduction/convection**

$$\rho_j c_{P,j} \frac{\partial T}{\partial t} = \lambda_j \operatorname{div} \operatorname{grad} T - \rho_j c_{P,j} \vec{u} \cdot \operatorname{grad} T \quad (2)$$

Momentum equation (**Navier Stokes**)

$$\rho_j \frac{\partial \vec{u}}{\partial t} + \rho_j \vec{u} \cdot \nabla \vec{u} = -\nabla p + \eta_j \nabla^2 \vec{u} \quad (3)$$

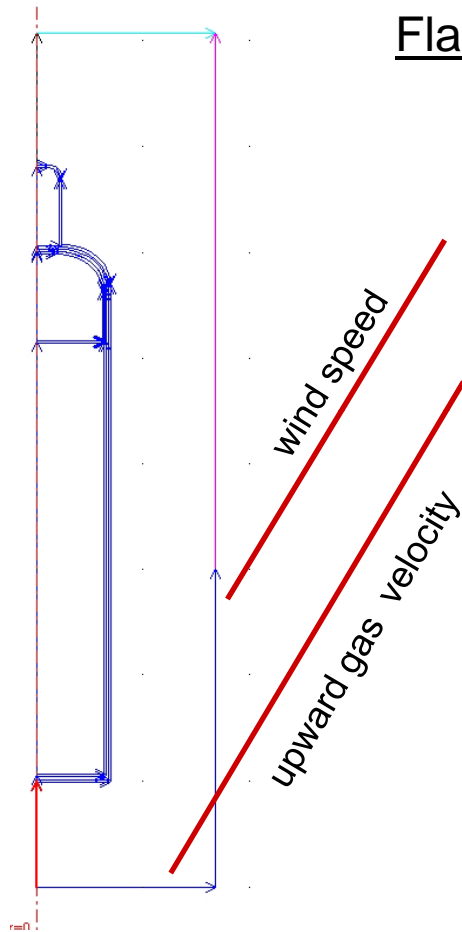
Continuity equation

$$\frac{\partial \rho_j}{\partial t} + \nabla \cdot (\rho_j \vec{u}) = 0 \quad (4)$$

j=1 air (heating up)

j=2 water (cooling)

Simulation: boundary settings (heating)



Flame velocity field

$$u = u(z) = -4u_{\max}z(1-z) \quad \text{or} \quad -u_{\max} \quad (5)$$

$$v = v(r) = 4v_{\max}r(1-r) \quad \text{or} \quad v_{\max} \quad (6)$$

Both currents are at $T_{\text{flame}} = 1000^{\circ}\text{C}$

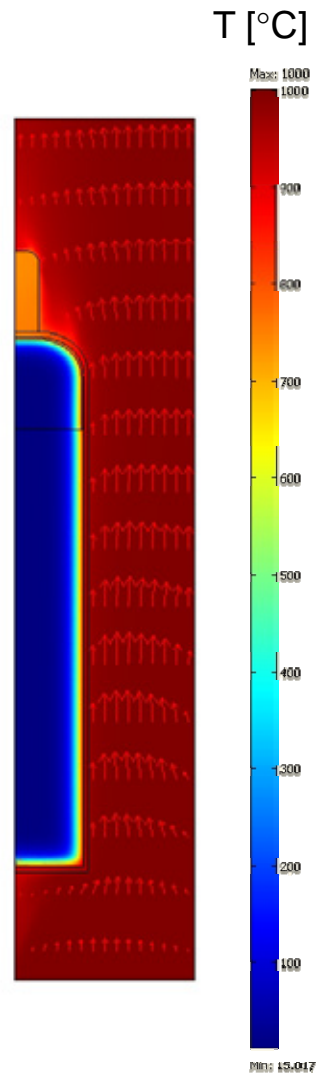
Simulation: results (heating)

Initial temperature: 15°C

$u_{\max} = 2 \text{ m/s}$

$v_{\max} = 5 \text{ m/s}$

$t = 1800 \text{ s}$



Simulation: results (heating)

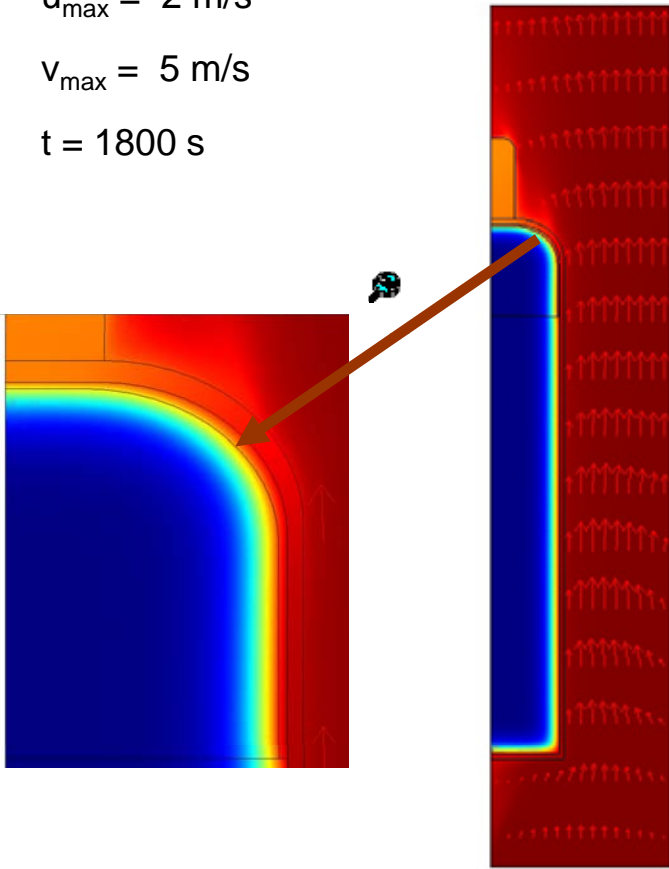
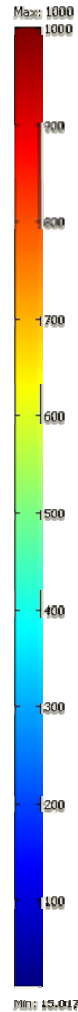
Initial temperature: 15°C

$u_{\max} = 2 \text{ m/s}$

$v_{\max} = 5 \text{ m/s}$

$t = 1800 \text{ s}$

T [°C]



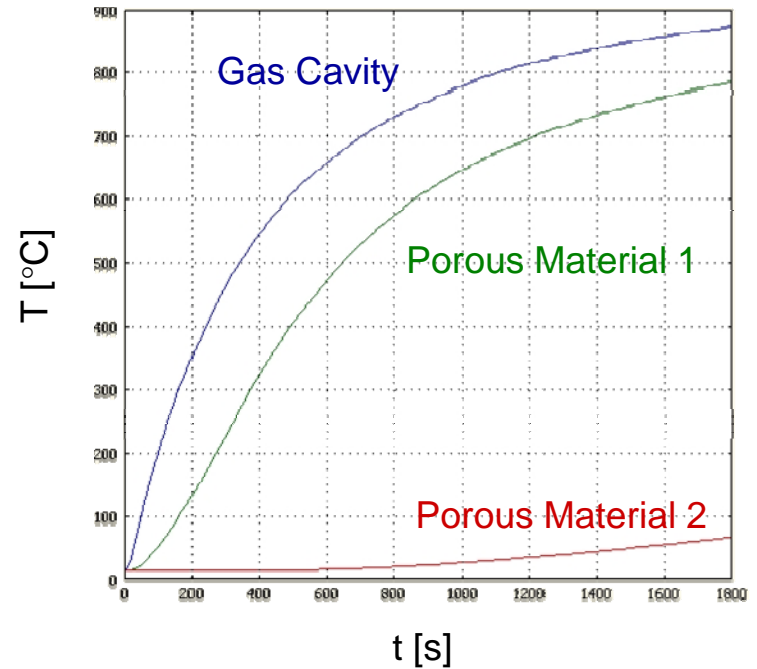
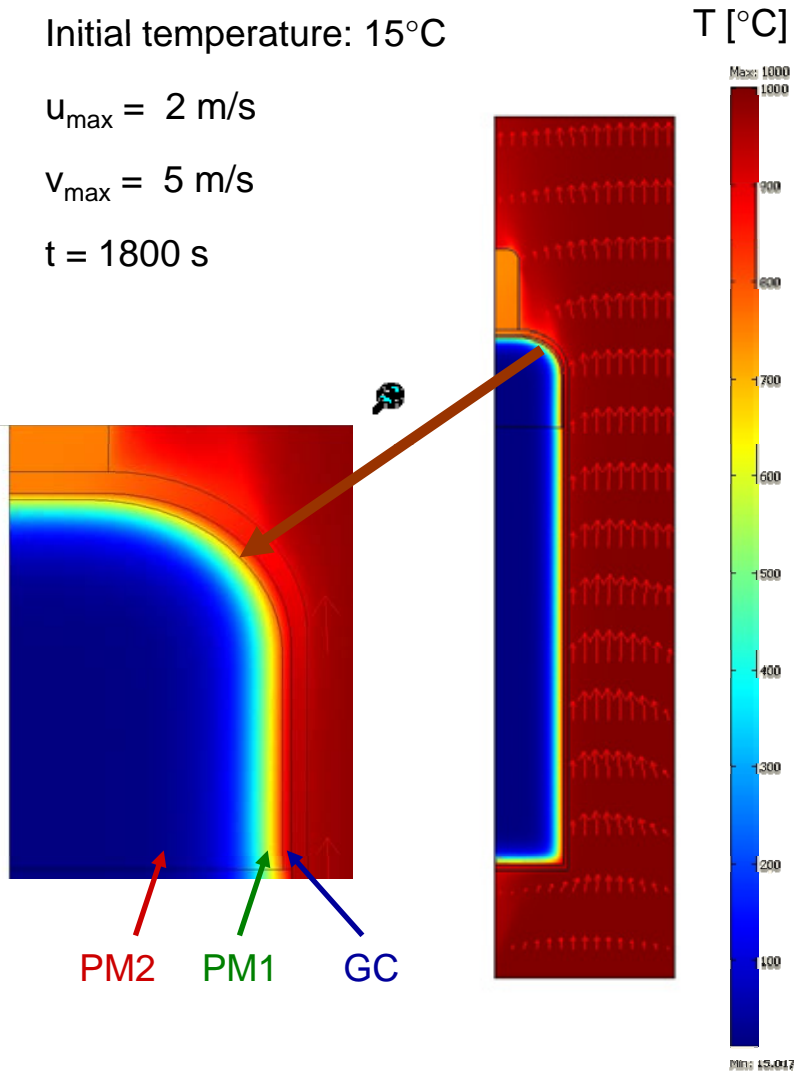
Simulation: results (heating)

Initial temperature: 15°C

$u_{\max} = 2 \text{ m/s}$

$v_{\max} = 5 \text{ m/s}$

$t = 1800 \text{ s}$



Critical temperatures
can be achieved

$p_0 = 10 \text{ bara}$, $T = 370^\circ\text{C}$
($V = 3 \text{ dm}^3$)

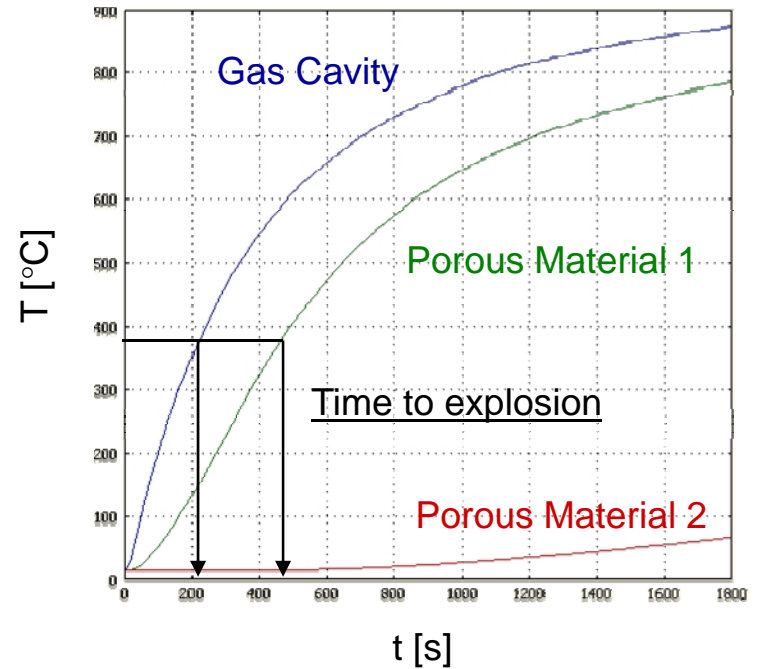
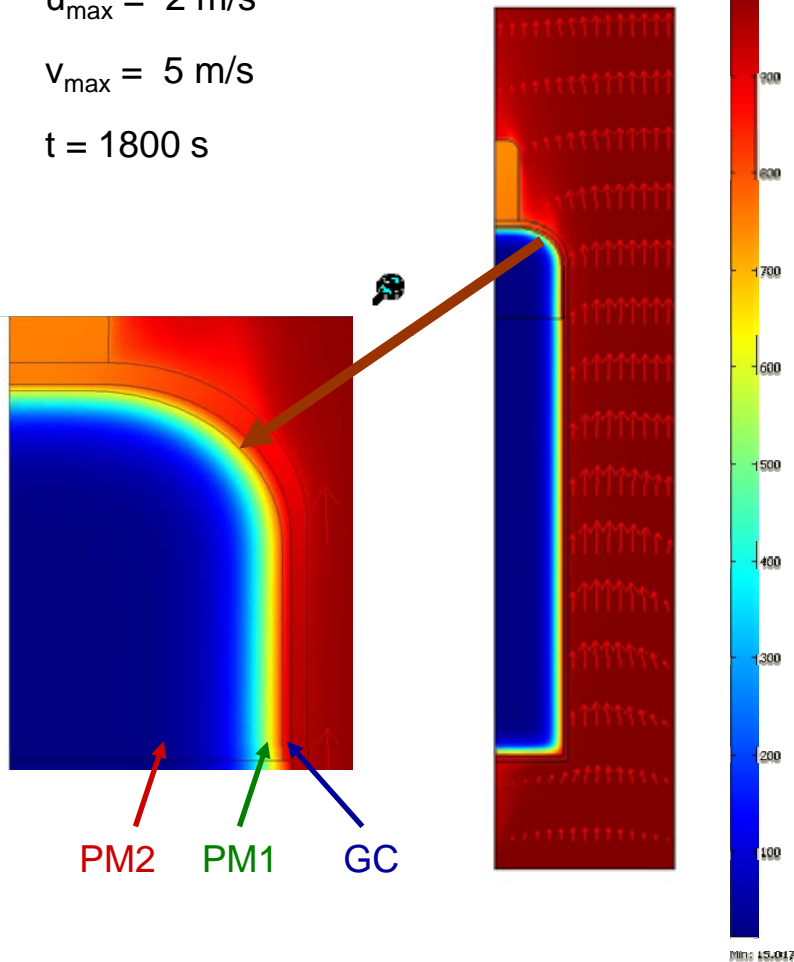
Simulation: results (heating)

Initial temperature: 15°C

$u_{\max} = 2 \text{ m/s}$

$v_{\max} = 5 \text{ m/s}$

$t = 1800 \text{ s}$



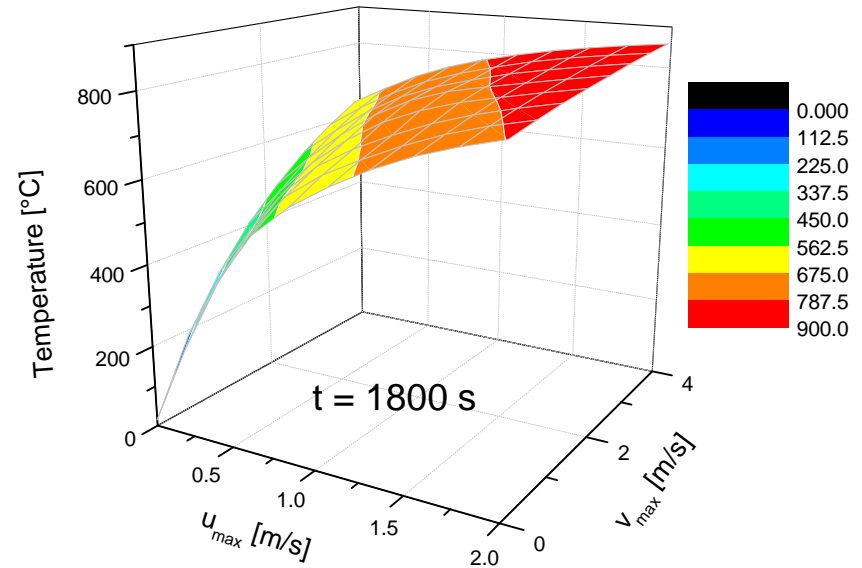
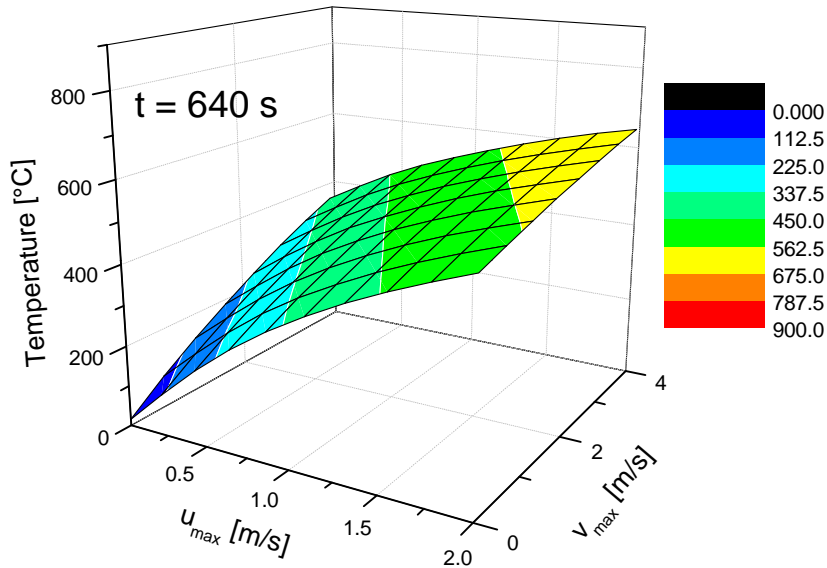
Critical temperatures
can be achieved

$p_0 = 10 \text{ bara}$, $T = 370^\circ\text{C}$
($V = 3 \text{ dm}^3$)

Simulation: results (heating)

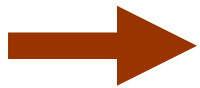
Temperature in the gas cavity as a function of:

- upward gas velocity (range 0-4 m/s)
- side wind speed (range 0-2 m/s)



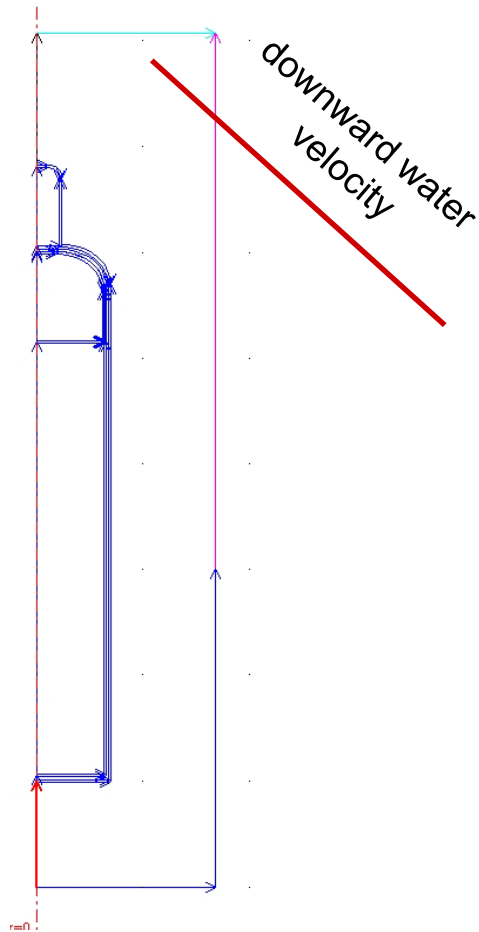
[initial temperature: 15°C]

Strong effects on the simulations



find optimum values

Simulation: boundary settings (cooling)

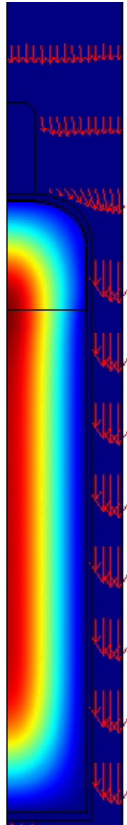


Water velocity field

$$v = v(r) = -4v_{\max}r(1-r) \quad \text{or } v_{\max} \quad (7)$$

The current is at $T_{\text{water}} = 20\text{-}80^{\circ}\text{C}$

Simulation: results (cooling)



$$v_{\max} = 1 \text{ m/s}$$

Initial temperature	Water temperature	Time to 350°C	Time to 300°C
[°C]	[°C]	[h]	[h]
400	20	10.1	13.8
400	30	10.3	14.1
400	80	10.5	15.5

Take with caution:

- 400°C may be too conservative
- include acetylene reaction (decomposition)

Conclusions / Future Work

Conclusions

COMSOL Multiphysics can help in increase the safe handling of acetylene cylinders involved in fire by predicting the:

- time to explosion due to fire exposure
- duration of the cooling with water after the fire

Future work

- comparison with experiments (some have been already performed)
- determination of critical temperatures/pressures for the decomposition
- inclusion of the pressure in the model
- inclusion of the decomposition reaction

COMSOL Multiphysics as a Tool to Increase Safety in the Handling of Acetylene Cylinders Involved in Fires

Fabio Ferrero

BAM Federal Institute for Materials Research and Testing
Division II.1 "Gases, Gas Plants"
Working Group "Safety Related Properties of Gases"
Unter den Eichen 87, D-12205 Berlin, Germany

COMSOL CONFERENCE
Milan, October 14-16 2009

